

SECTION XI

Rules for Inservice Inspection of
Nuclear Power Plant Components

2021

ASME Boiler and
Pressure Vessel Code
An International Code

Division 2

Requirements for Reliability and
Integrity Management (RIM)
Programs for Nuclear Power Plants

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AN INTERNATIONAL CODE

2021 ASME Boiler & Pressure Vessel Code

2021 Edition

July 1, 2021

XI

RULES FOR INSERVICE INSPECTION OF NUCLEAR POWER PLANT COMPONENTS

Division 2

Requirements for Reliability and Integrity Management (RIM) Programs for Nuclear Power Plants

ASME Boiler and Pressure Vessel Committee
on Nuclear Inservice Inspection



The American Society of
Mechanical Engineers

Two Park Avenue • New York, NY • 10016 USA

Date of Issuance: July 1, 2021

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Library of Congress Catalog Card Number: 56-3934
Printed in the United States of America

Adopted by the Council of The American Society of Mechanical Engineers, 1914; latest edition 2021.

The American Society of Mechanical Engineers
Two Park Avenue, New York, NY 10016-5990

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* In the 2021 Edition, Subsections NC and ND have been incorporated into one publication, Subsection NCD (BPVC.III.1.NCD), Class 2 and Class 3 Components.

INTERPRETATIONS

Interpretations are issued in real time in ASME's Interpretations Database at <http://go.asme.org/Interpretations>. Historical BPVC interpretations may also be found in the Database.

CODE CASES

The Boiler and Pressure Vessel Code committees meet regularly to consider proposed additions and revisions to the Code and to formulate Cases to clarify the intent of existing requirements or provide, when the need is urgent, rules for materials or constructions not covered by existing Code rules. Those Cases that have been adopted will appear in the appropriate 2021 Code Cases book: "Boilers and Pressure Vessels" or "Nuclear Components." Each Code Cases book is updated with seven Supplements. Supplements will be sent or made available automatically to the purchasers of the Code Cases books up to the publication of the 2023 Code. Annulments of Code Cases become effective six months after the first announcement of the annulment in a Code Case Supplement or Edition of the appropriate Code Case book. Code Case users can check the current status of any Code Case at <http://go.asme.org/BPVCCDatabase>. Code Case users can also view an index of the complete list of Boiler and Pressure Vessel Code Cases and Nuclear Code Cases at <http://go.asme.org/BPVCC>.

FOREWORD*

In 1911, The American Society of Mechanical Engineers established the Boiler and Pressure Vessel Committee to formulate standard rules for the construction of steam boilers and other pressure vessels. In 2009, the Boiler and Pressure Vessel Committee was superseded by the following committees:

- (a) Committee on Power Boilers (I)
- (b) Committee on Materials (II)
- (c) Committee on Construction of Nuclear Facility Components (III)
- (d) Committee on Heating Boilers (IV)
- (e) Committee on Nondestructive Examination (V)
- (f) Committee on Pressure Vessels (VIII)
- (g) Committee on Welding, Brazing, and Fusing (IX)
- (h) Committee on Fiber-Reinforced Plastic Pressure Vessels (X)
- (i) Committee on Nuclear Inservice Inspection (XI)
- (j) Committee on Transport Tanks (XII)
- (k) Committee on Overpressure Protection (XIII)
- (l) Technical Oversight Management Committee (TOMC)

Where reference is made to “the Committee” in this Foreword, each of these committees is included individually and collectively.

The Committee’s function is to establish rules of safety relating to pressure integrity, which govern the construction** of boilers, pressure vessels, transport tanks, and nuclear components, and the inservice inspection of nuclear components and transport tanks. For nuclear items other than pressure-retaining components, the Committee also establishes rules of safety related to structural integrity. The Committee also interprets these rules when questions arise regarding their intent. The technical consistency of the Sections of the Code and coordination of standards development activities of the Committees is supported and guided by the Technical Oversight Management Committee. This Code does not address other safety issues relating to the construction of boilers, pressure vessels, transport tanks, or nuclear components, or the inservice inspection of nuclear components or transport tanks. Users of the Code should refer to the pertinent codes, standards, laws, regulations, or other relevant documents for safety issues other than those relating to pressure integrity and, for nuclear items other than pressure-retaining components, structural integrity. Except for Sections XI and XII, and with a few other exceptions, the rules do not, of practical necessity, reflect the likelihood and consequences of deterioration in service related to specific service fluids or external operating environments. In formulating the rules, the Committee considers the needs of users, manufacturers, and inspectors of components addressed by the Code. The objective of the rules is to afford reasonably certain protection of life and property, and to provide a margin for deterioration in service to give a reasonably long, safe period of usefulness. Advancements in design and materials and evidence of experience have been recognized.

This Code contains mandatory requirements, specific prohibitions, and nonmandatory guidance for construction activities and inservice inspection and testing activities. The Code does not address all aspects of these activities and those aspects that are not specifically addressed should not be considered prohibited. The Code is not a handbook and cannot replace education, experience, and the use of engineering judgment. The phrase *engineering judgment* refers to technical judgments made by knowledgeable engineers experienced in the application of the Code. Engineering judgments must be consistent with Code philosophy, and such judgments must never be used to overrule mandatory requirements or specific prohibitions of the Code.

The Committee recognizes that tools and techniques used for design and analysis change as technology progresses and expects engineers to use good judgment in the application of these tools. The designer is responsible for complying with Code rules and demonstrating compliance with Code equations when such equations are mandatory. The Code neither requires nor prohibits the use of computers for the design or analysis of components constructed to the requirements of the Code. However, designers and engineers using computer programs for design or analysis are cautioned that they are

* The information contained in this Foreword is not part of this American National Standard (ANS) and has not been processed in accordance with ANSI’s requirements for an ANS. Therefore, this Foreword may contain material that has not been subjected to public review or a consensus process. In addition, it does not contain requirements necessary for conformance to the Code.

** *Construction*, as used in this Foreword, is an all-inclusive term comprising materials, design, fabrication, examination, inspection, testing, certification, and overpressure protection.

responsible for all technical assumptions inherent in the programs they use and the application of these programs to their design.

The rules established by the Committee are not to be interpreted as approving, recommending, or endorsing any proprietary or specific design, or as limiting in any way the manufacturer's freedom to choose any method of design or any form of construction that conforms to the Code rules.

The Committee meets regularly to consider revisions of the rules, new rules as dictated by technological development, Code Cases, and requests for interpretations. Only the Committee has the authority to provide official interpretations of this Code. Requests for revisions, new rules, Code Cases, or interpretations shall be addressed to the Secretary in writing and shall give full particulars in order to receive consideration and action (see Submittal of Technical Inquiries to the Boiler and Pressure Vessel Standards Committees). Proposed revisions to the Code resulting from inquiries will be presented to the Committee for appropriate action. The action of the Committee becomes effective only after confirmation by ballot of the Committee and approval by ASME. Proposed revisions to the Code approved by the Committee are submitted to the American National Standards Institute (ANSI) and published at <http://go.asme.org/BPVCPublicReview> to invite comments from all interested persons. After public review and final approval by ASME, revisions are published at regular intervals in Editions of the Code.

The Committee does not rule on whether a component shall or shall not be constructed to the provisions of the Code. The scope of each Section has been established to identify the components and parameters considered by the Committee in formulating the Code rules.

Questions or issues regarding compliance of a specific component with the Code rules are to be directed to the ASME Certificate Holder (Manufacturer). Inquiries concerning the interpretation of the Code are to be directed to the Committee. ASME is to be notified should questions arise concerning improper use of the ASME Single Certification Mark.

When required by context in this Section, the singular shall be interpreted as the plural, and vice versa, and the feminine, masculine, or neuter gender shall be treated as such other gender as appropriate.

The words "shall," "should," and "may" are used in this Standard as follows:

- *Shall* is used to denote a requirement.
- *Should* is used to denote a recommendation.
- *May* is used to denote permission, neither a requirement nor a recommendation.

STATEMENT OF POLICY ON THE USE OF THE ASME SINGLE CERTIFICATION MARK AND CODE AUTHORIZATION IN ADVERTISING

ASME has established procedures to authorize qualified organizations to perform various activities in accordance with the requirements of the ASME Boiler and Pressure Vessel Code. It is the aim of the Society to provide recognition of organizations so authorized. An organization holding authorization to perform various activities in accordance with the requirements of the Code may state this capability in its advertising literature.

Organizations that are authorized to use the ASME Single Certification Mark for marking items or constructions that have been constructed and inspected in compliance with the ASME Boiler and Pressure Vessel Code are issued Certificates of Authorization. It is the aim of the Society to maintain the standing of the ASME Single Certification Mark for the benefit of the users, the enforcement jurisdictions, and the holders of the ASME Single Certification Mark who comply with all requirements.

Based on these objectives, the following policy has been established on the usage in advertising of facsimiles of the ASME Single Certification Mark, Certificates of Authorization, and reference to Code construction. The American Society of Mechanical Engineers does not “approve,” “certify,” “rate,” or “endorse” any item, construction, or activity and there shall be no statements or implications that might so indicate. An organization holding the ASME Single Certification Mark and/or a Certificate of Authorization may state in advertising literature that items, constructions, or activities “are built (produced or performed) or activities conducted in accordance with the requirements of the ASME Boiler and Pressure Vessel Code,” or “meet the requirements of the ASME Boiler and Pressure Vessel Code.” An ASME corporate logo shall not be used by any organization other than ASME.

The ASME Single Certification Mark shall be used only for stamping and nameplates as specifically provided in the Code. However, facsimiles may be used for the purpose of fostering the use of such construction. Such usage may be by an association or a society, or by a holder of the ASME Single Certification Mark who may also use the facsimile in advertising to show that clearly specified items will carry the ASME Single Certification Mark.

STATEMENT OF POLICY ON THE USE OF ASME MARKING TO IDENTIFY MANUFACTURED ITEMS

The ASME Boiler and Pressure Vessel Code provides rules for the construction of boilers, pressure vessels, and nuclear components. This includes requirements for materials, design, fabrication, examination, inspection, and stamping. Items constructed in accordance with all of the applicable rules of the Code are identified with the ASME Single Certification Mark described in the governing Section of the Code.

Markings such as “ASME,” “ASME Standard,” or any other marking including “ASME” or the ASME Single Certification Mark shall not be used on any item that is not constructed in accordance with all of the applicable requirements of the Code.

Items shall not be described on ASME Data Report Forms nor on similar forms referring to ASME that tend to imply that all Code requirements have been met when, in fact, they have not been. Data Report Forms covering items not fully complying with ASME requirements should not refer to ASME or they should clearly identify all exceptions to the ASME requirements.

SUBMITTAL OF TECHNICAL INQUIRIES TO THE BOILER AND PRESSURE VESSEL STANDARDS COMMITTEES

(21)

1 INTRODUCTION

(a) The following information provides guidance to Code users for submitting technical inquiries to the applicable Boiler and Pressure Vessel (BPV) Standards Committee (hereinafter referred to as the Committee). See the guidelines on approval of new materials under the ASME Boiler and Pressure Vessel Code in Section II, Part D for requirements for requests that involve adding new materials to the Code. See the guidelines on approval of new welding and brazing materials in Section II, Part C for requirements for requests that involve adding new welding and brazing materials ("consumables") to the Code.

Technical inquiries can include requests for revisions or additions to the Code requirements, requests for Code Cases, or requests for Code Interpretations, as described below:

(1) *Code Revisions*. Code revisions are considered to accommodate technological developments, to address administrative requirements, to incorporate Code Cases, or to clarify Code intent.

(2) *Code Cases*. Code Cases represent alternatives or additions to existing Code requirements. Code Cases are written as a Question and Reply, and are usually intended to be incorporated into the Code at a later date. When used, Code Cases prescribe mandatory requirements in the same sense as the text of the Code. However, users are cautioned that not all regulators, jurisdictions, or Owners automatically accept Code Cases. The most common applications for Code Cases are as follows:

- (-a) to permit early implementation of an approved Code revision based on an urgent need
- (-b) to permit use of a new material for Code construction
- (-c) to gain experience with new materials or alternative requirements prior to incorporation directly into the Code

(3) *Code Interpretations*

(-a) Code Interpretations provide clarification of the meaning of existing requirements in the Code and are presented in Inquiry and Reply format. Interpretations do not introduce new requirements.

(-b) Interpretations will be issued only if existing Code text is ambiguous or conveys conflicting requirements. If a revision of the requirements is required to support the Interpretation, an Intent Interpretation will be issued in parallel with a revision to the Code.

(b) Code requirements, Code Cases, and Code Interpretations established by the Committee are not to be considered as approving, recommending, certifying, or endorsing any proprietary or specific design, or as limiting in any way the freedom of manufacturers, constructors, or Owners to choose any method of design or any form of construction that conforms to the Code requirements.

(c) Inquiries that do not comply with the following guidance or that do not provide sufficient information for the Committee's full understanding may result in the request being returned to the Inquirer with no action.

2 INQUIRY FORMAT

Submittals to the Committee should include the following information:

(a) *Purpose*. Specify one of the following:

- (1) request for revision of present Code requirements
- (2) request for new or additional Code requirements
- (3) request for Code Case
- (4) request for Code Interpretation

(b) *Background*. The Inquirer should provide the information needed for the Committee's understanding of the Inquiry, being sure to include reference to the applicable Code Section, Division, Edition, Addenda (if applicable), paragraphs, figures, and tables. This information should include a statement indicating why the included paragraphs, figures, or tables are ambiguous or convey conflicting requirements. Preferably, the Inquirer should provide a copy of, or relevant extracts from, the specific referenced portions of the Code.

(c) *Presentations.* The Inquirer may desire to attend or be asked to attend a meeting of the Committee to make a formal presentation or to answer questions from the Committee members with regard to the Inquiry. Attendance at a BPV Standards Committee meeting shall be at the expense of the Inquirer. The Inquirer's attendance or lack of attendance at a meeting will not be used by the Committee as a basis for acceptance or rejection of the Inquiry by the Committee. However, if the Inquirer's request is unclear, attendance by the Inquirer or a representative may be necessary for the Committee to understand the request sufficiently to be able to provide an Interpretation. If the Inquirer desires to make a presentation at a Committee meeting, the Inquirer should provide advance notice to the Committee Secretary, to ensure time will be allotted for the presentation in the meeting agenda. The Inquirer should consider the need for additional audiovisual equipment that might not otherwise be provided by the Committee. With sufficient advance notice to the Committee Secretary, such equipment may be made available.

3 CODE REVISIONS OR ADDITIONS

Requests for Code revisions or additions should include the following information:

(a) *Requested Revisions or Additions.* For requested revisions, the Inquirer should identify those requirements of the Code that they believe should be revised, and should submit a copy of, or relevant extracts from, the appropriate requirements as they appear in the Code, marked up with the requested revision. For requested additions to the Code, the Inquirer should provide the recommended wording and should clearly indicate where they believe the additions should be located in the Code requirements.

(b) *Statement of Need.* The Inquirer should provide a brief explanation of the need for the revision or addition.

(c) *Background Information.* The Inquirer should provide background information to support the revision or addition, including any data or changes in technology that form the basis for the request, that will allow the Committee to adequately evaluate the requested revision or addition. Sketches, tables, figures, and graphs should be submitted, as appropriate. The Inquirer should identify any pertinent portions of the Code that would be affected by the revision or addition and any portions of the Code that reference the requested revised or added paragraphs.

4 CODE CASES

Requests for Code Cases should be accompanied by a statement of need and background information similar to that described in 3(b) and 3(c), respectively, for Code revisions or additions. The urgency of the Code Case (e.g., project underway or imminent, new procedure) should be described. In addition, it is important that the request is in connection with equipment that will bear the ASME Single Certification Mark, with the exception of Section XI applications. The proposed Code Case should identify the Code Section and Division, and should be written as a Question and a Reply, in the same format as existing Code Cases. Requests for Code Cases should also indicate the applicable Code Editions and Addenda (if applicable) to which the requested Code Case applies.

5 CODE INTERPRETATIONS

(a) Requests for Code Interpretations should be accompanied by the following information:

(1) *Inquiry.* The Inquirer should propose a condensed and precise Inquiry, omitting superfluous background information and, when possible, composing the Inquiry in such a way that a "yes" or a "no" Reply, with brief limitations or conditions, if needed, can be provided by the Committee. The proposed question should be technically and editorially correct.

(2) *Reply.* The Inquirer should propose a Reply that clearly and concisely answers the proposed Inquiry question. Preferably, the Reply should be "yes" or "no," with brief limitations or conditions, if needed.

(3) *Background Information.* The Inquirer should include a statement indicating why the included paragraphs, figures, or tables are ambiguous or convey conflicting requirements. The Inquirer should provide any need or background information, such as described in 3(b) and 3(c), respectively, for Code revisions or additions, that will assist the Committee in understanding the proposed Inquiry and Reply.

If the Inquirer believes a revision of the Code requirements would be helpful to support the Interpretation, the Inquirer may propose such a revision for consideration by the Committee. In most cases, such a proposal is not necessary.

(b) Requests for Code Interpretations should be limited to an Interpretation of a particular requirement in the Code or in a Code Case. Except with regard to interpreting a specific Code requirement, the Committee is not permitted to consider consulting-type requests such as the following:

(1) a review of calculations, design drawings, welding qualifications, or descriptions of equipment or parts to determine compliance with Code requirements

(2) a request for assistance in performing any Code-prescribed functions relating to, but not limited to, material selection, designs, calculations, fabrication, inspection, pressure testing, or installation

(3) a request seeking the rationale for Code requirements

6 SUBMITTALS

(a) *Submittal.* Requests for Code Interpretation should preferably be submitted through the online Interpretation Submittal Form. The form is accessible at <http://go.asme.org/InterpretationRequest>. Upon submittal of the form, the Inquirer will receive an automatic e-mail confirming receipt. If the Inquirer is unable to use the online form, the Inquirer may mail the request to the following address:

Secretary
ASME Boiler and Pressure Vessel Committee
Two Park Avenue
New York, NY 10016-5990

All other Inquiries should be mailed to the Secretary of the BPV Committee at the address above. Inquiries are unlikely to receive a response if they are not written in clear, legible English. They must also include the name of the Inquirer and the company they represent or are employed by, if applicable, and the Inquirer's address, telephone number, fax number, and e-mail address, if available.

(b) *Response.* The Secretary of the appropriate Committee will provide a written response, via letter or e-mail, as appropriate, to the Inquirer, upon completion of the requested action by the Committee. Inquirers may track the status of their Interpretation Request at <http://go.asme.org/Interpretations>.

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January 1, 2021

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PREFACE TO SECTION XI

INTRODUCTION

Section XI, Division 1, Rules for Inspection and Testing of Components of Light-Water-Cooled Plants, of the ASME Boiler and Pressure Vessel Code provides requirements for examination, testing, and inspection of components and systems, and repair/replacement activities in a nuclear power plant. Application of Division 1 begins when the requirements of the Construction Code have been satisfied.

Section XI, Division 2, Requirements for Reliability and Integrity Management (RIM) Programs for Nuclear Power Plants, is a technology-neutral standard of the ASME Boiler and Pressure Vessel Code. It provides requirements for protecting pressure integrity of structures, systems, and components (SSCs) that affect reliability. Application of Division 2 begins when the requirements of the Construction Code have been satisfied. It is applicable regardless of the Construction Code classification used for an SSC if the SSC is designated as important to the safety and reliability of an operating plant.

GENERAL

The rules of this Section constitute requirements to maintain the nuclear power plant and to return the plant to service, following plant outages, in a safe and expeditious manner.

Division 1 rules require a mandatory program of examinations, testing, and inspections to evidence adequate safety and to manage deterioration and aging effects. The rules also stipulate duties of the Authorized Nuclear Inservice Inspector to verify that the mandatory program has been completed, permitting the plant to return to service in an expeditious manner.

Division 2 rules require the development of a Reliability and Integrity Management (RIM) Program that considers the combination of design, fabrication, degradation mechanisms, inspection, examination, monitoring, operation, and maintenance of SSCs to ensure they will meet their required reliability target values. The rules also stipulate duties of the Authorized Nuclear Inservice Inspector to verify that the program has been completed, implemented, and updated in accordance with the requirements of Division 2.

INSERVICE TESTING OF PUMP AND VALVES

With the 1998 Edition with the 2000 Addenda, all requirements for testing pumps and valves have been removed from Section XI, Division 1. These requirements are now located in the ASME Code for Operation and Maintenance of Nuclear Power Plants.

OWNER RESPONSIBILITIES

The Owner of the nuclear power plant is assigned the responsibilities to develop a program which will demonstrate conformance to the requirements of this Section of the Code. These responsibilities include:

- (a) provision of access in the design and arrangement of the plant to conduct the examination and tests;
- (b) development of plans and schedules, including detailed examination and testing procedures;
- (c) conduct of the program of examination and tests, system leakage and hydrostatic pressure tests; and
- (d) recording of the results of the examinations and tests, including corrective actions required and the actions taken.

DUTIES OF THE AUTHORIZED NUCLEAR INSERVICE INSPECTOR

Section XI differs from Section VI, Recommended Rules for the Care and Operation of Heating Boilers, and Section VII, Recommended Guidelines for the Care of Power Boilers, in that the requirements for Inservice Inspection of Nuclear Power Plants are mandatory, while the other two Sections are recommended practices. Duties of the Authorized Nuclear Inservice Inspector are assigned by Section XI to verify that the responsibilities of the Owner and the mandatory requirements of this Section are met. Duties of the Authorized Nuclear Inservice Inspector include the following:

- (a) verifying system pressure tests;
- (b) reviewing nondestructive examination procedures and Repair/Replacement Programs and Plans; and
- (c) verifying that the visual examinations and tests have been completed and the results recorded.

Listed as one of the duties is the prerogative of the Inspector to require requalification of any operator or procedure when he has reason to believe the requirements are not being met.

ORGANIZATION OF SECTION XI

1 DIVISIONS

Section XI consists of two Divisions, as follows:

Division 1 = Rules for Inspection and Testing of Components of Light-Water-Cooled Plants

Division 2 = Requirements for Reliability and Integrity Management (RIM) Programs for Nuclear Power Plants

2 ORGANIZATION OF DIVISION 1

2.1 SUBSECTIONS

Division 1 is broken down into Subsections that are designated by capital letters, preceded by the letters IW. Division 1 consists of Subsections covering the following aspects of the rules:

Subsection	Title
IWA	General Requirements
IWB	Class 1 Components
IWC	Class 2 Components
IWD	Class 3 Components
IWE	Class MC and CC Components
IWF	Class 1, 2, 3, and MC Component Supports
IWG	Core Internal Structures (In course of preparation)
IWL	Class CC Concrete Components

Subsections are divided into Articles, subarticles, paragraphs, and, where necessary, into subparagraphs.

2.2 ARTICLES

Articles are designated by the applicable letters indicated above for the Subsections, followed by Arabic numbers, such as IWA-1000 or IWB-2000. Where possible, Articles dealing with the same general topics are given the same number in each Subsection, in accordance with the following scheme:

Article Number	Title
1000	Scope and Responsibility
2000	Examination and Inspection
3000	Acceptance Standards
4000	Repair/Replacement Activities
5000	System Pressure Tests
6000	Records and Reports

The numbering of Articles and material contained in the Articles may not, however, be consecutive. Due to the fact that the complete outline may cover phases not applicable to a particular Subsection or Article, the requirements have been prepared with some gaps in the numbering.

2.3 SUBARTICLES

Subarticles are numbered in units of 100, such as IWA-1100 or IWA-1200.

2.4 SUBSUBARTICLES

Subsubarticles are numbered in units of 10, such as IWA-2130, and may have no text. When a number such as IWA-1110 is followed by text, it is considered a paragraph.

2.5 PARAGRAPHS

Paragraphs are numbered in units of 1, such as IWA-2131 or IWA-2132.

2.6 SUBPARAGRAPHS

Subparagraphs, when they are *major* subdivisions of a paragraph, are designated by adding a decimal followed by one or more digits to the paragraph number, such as IWA-1111.1 or IWA-1111.2. When they are *minor* subdivisions of a paragraph, subparagraphs may be designated by lowercase letters in parentheses, such as IWA-1111(a) or IWA-1111(b).

3 ORGANIZATION OF DIVISION 2

Division 2 is broken down into Articles that are designated by the capital letters RIM, followed by the Article number. Division 2 Articles consist of the following:

Article	Title
RIM-1	Scope and Responsibility
RIM-2	Reliability and Integrity Management (RIM) Program
RIM-3	Acceptance Standards
RIM-4	Repair/Replacement Activities
RIM-5	System Leak Monitoring and Periodic Tests
RIM-6	Records and Reports
RIM-7	Glossary

Division 2 also maintains Mandatory Appendices that are required for the development and implementation of the RIM Program. Mandatory Appendices consist of the following:

Appendix	Title
I	RIM Decision Flowcharts for Use With the RIM Program
II	Derivation of Component Reliability Targets From Plant Safety Requirements
III	Owner's Record and Report for RIM Program Activities
IV	Monitoring and NDE Qualification
V	Catalog of NDE Requirements and Areas of Interest
VI	Reliability and Integrity Management Expert Panel (RIMEP)
VII	Supplements for Types of Nuclear Plants

Articles are divided into paragraphs and subparagraphs. Appendices are divided into Articles, paragraphs, and subparagraphs.

4 REFERENCES

References used within this Section generally fall into one of six categories, as explained below.

(a) *References to Other Portions of This Section.* When a reference is made to another Article, Subarticle, or paragraph number, all numbers subsidiary to that reference shall be included. For example, reference to IWA-2000 includes all materials in Article IWA-2000; reference to IWA-2200 includes all material in Subarticle IWA-2200; reference to IWA-2220 includes all paragraphs in IWA-2220, IWA-2221, and IWA-2222.

(b) *References to Other Sections.* Other Sections referred to in Section XI are as follows:

(1) *Section II, Material Specifications.* When a requirement for a material or for the examination or testing of a material is to be in accordance with a specification such as SA-105, SA-370, or SB-160, the reference is to material specifications in Section II. These references begin with the letter “S.” Materials conforming to ASTM specifications may be used in accordance with the provisions of the last paragraph of the Foreword to the Boiler Code.

(2) *Section III, Nuclear Power Plant Components.* Section III references begin with the letter “N” and relate to nuclear power plant design or construction requirements.

(3) *Section V, Nondestructive Examination.* Section V references begin with the letter “T” and relate to the non-destructive examination of material or welds.

(4) *Section IX, Welding and Brazing Qualifications.* Section IX references begin with the letter “Q” and relate to welding and brazing requirements.

(c) *References to Specifications and Standards Other Than Published in Code Sections*

(1) Specifications for examination methods and acceptance standards to be used in connection with them are published by the American Society for Testing and Materials. For example, reference to ASTM E71-64 refers to the specification so designated and published by American Society for Testing and Materials (ASTM), 100 Barr Harbor Drive, West Conshohocken, PA 19428.

(2) Recommended practices for qualifying and certifying nondestructive examination personnel are published by the American Society for Nondestructive Testing (ASNT). These documents are designated SNT-TC-1A and CP-189. A reference to SNT-TC-1A or CP-189 shall be understood to mean the practice and its supplements, so designated and published by the American Society for Nondestructive Testing (ASNT), 1711 Arlingate Lane, P. O. Box 28518, Columbus, OH 43228-0518.

(3) Specifications and standards for materials, processes, examination and test procedures, qualifications of personnel, and other requirements of the Code approved by the American National Standards Institute are designated by the letters ANSI followed by the serialization for the particular specification or standard. Standards published by ASME are available from ASME (<https://www.asme.org/>).

(4) Specifications and standards for materials, processes, examination and test procedures, and other requirements of the Code relating to concrete are listed in Table IWA-1600-1, designated by the letters ACI, and are approved and published by the American Concrete Institute. Standards published by the American Concrete Institute can be obtained by writing ACI, Box 19150, 22400 West Seven Mile Road, Detroit, MI 48219.

(5) Specifications and standards for determining water chemistry as identified in Table IWA-1600-1 by the letter designation APHA are approved and published by the American Public Health Association. Standards published by the American Public Health Association can be obtained by writing APHA, 1015 15th Street, NW, Washington, D.C. 20005.

(6) Specifications and standards for welding are listed in Table IWA-1600-1 and are approved and published by the American Welding Society. Standards published by the American Welding Society can be obtained by writing AWS, 8669 NW 36 Street, No. 130, Miami, FL 33166.

(d) *References to Government Regulations.* U.S. Federal regulations issued by executive departments and agencies, as published in the Federal Register, are codified in the Code of Federal Regulations. The Code of Federal Regulations is published by the Office of the Federal Register, National Archives and Records Service, General Service Administration, and may be purchased from the Superintendent of Documents, U.S. Government Printing Office, Washington, D.C. 20402. Title 10 of the Code of Federal Regulations contains the regulations for atomic energy. The abbreviated reference “10 CFR 50” is used to mean “Title 10, Code of Federal Regulations, Part 50.”

(e) *References to Appendices.* Two types of Appendices are used in Section XI and are designated Mandatory and Nonmandatory.

(1) Mandatory Appendices contain requirements which must be followed in Section XI activities; such references are designated by a Roman numeral followed by Arabic numerals. A reference to III-1100, for example, refers to a Mandatory Appendix.

(2) Nonmandatory Appendices provide information or guidance for the use of Section XI; such references are designated by a capital letter followed by Arabic numerals. A reference to A-3300, for example, refers to a Nonmandatory Appendix.

(f) *References to Technical Reports.* The following reports prepared at the request of the American Society of Mechanical Engineers and published by Electric Power Research Institute are relevant to Code-related articles of Section XI. Requests for copies should be directed to EPRI Research Reports Center, Box 50490, Palo Alto, CA 94303.

(1) NP-1406-SR — Nondestructive Examination Acceptance Standards Technical Basis and Development for Boiler and Pressure Vessel Code, ASME Section XI, Division 1, Special Report, May 1980.

(2) NP-719-SR — Flaw Evaluation Procedures — Background and Application of ASME Section XI Appendix A — Special Report, August 1978.

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SUMMARY OF CHANGES

Errata to the BPV Code may be posted on the ASME website to provide corrections to incorrectly published items, or to correct typographical or grammatical errors in the BPV Code. Such Errata shall be used on the date posted.

Information regarding Special Notices and Errata is published by ASME at <http://go.asme.org/BPVCerrata>.

Changes given below are identified on the pages by a margin note, **(21)**, placed next to the affected area.

<i>Page</i>	<i>Location</i>	<i>Change</i>
viii	List of Sections	(1) Listing for Section III updated (2) Section XIII added (3) Code Case information updated
x	Foreword	(1) Subparagraph (k) added and subsequent subparagraph redesignated (2) Second footnote revised (3) Last paragraph added
xiii	Submittal of Technical Inquiries to the Boiler and Pressure Vessel Standards Committees	Paragraphs 1(a)(3)(-b), 2(b), and 5(a)(3) revised
xvi	Personnel	Updated
2	RIM-1.6.1	(1) Title revised (2) New subparas. (a) and (b) added and subsequent subparagraphs redesignated (3) Subparagraph (c) editorially revised
4	RIM-2.1.1	In subpara. (d), cross-references to figures updated
13	RIM-4.1	Subparagraph (c) added
18	RIM-7.1	Definitions of <i>MANDE Program</i> and <i>RIM Program</i> added
20	I-1.1	Revised
21	Figure I-1.1-1	Revised in its entirety
22	Figure I-1.1-2	Revised in its entirety
23	Figure I-1.1-3	Revised in its entirety
24	Figure I-1.1-4	Revised in its entirety
25	Figure I-1.1-5	Revised in its entirety
26	Figure I-1.1-6	Revised in its entirety
27	Figure I-1.1-7	Deleted
31	Table III-1.1-1	Last entry added
32	IV-1.1	In last sentence, cross-reference to figures updated
32	IV-1.3.2.1	In subpara. (a), cross-reference updated
34	IV-2.1	In title, cross-reference updated
35	IV-3.3.2	In title, cross-reference updated
63	VII-1.5	Subparagraphs (a) through (d) added
64	VII-1.5.1	Revised
65	VII-1.5.3	Revised
81	VII-3.5	Subparagraphs (a) through (d) added
81	VII-3.5.1	Revised
82	VII-3.5.3	Revised

LIST OF CHANGES IN RECORD NUMBER ORDER

DELETED

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CROSS-REFERENCING AND STYLISTIC CHANGES IN THE BOILER AND PRESSURE VESSEL CODE

There have been structural and stylistic changes to BPVC, starting with the 2011 Addenda, that should be noted to aid navigating the contents. The following is an overview of the changes:

Subparagraph Breakdowns/Nested Lists Hierarchy

- First-level breakdowns are designated as (a), (b), (c), etc., as in the past.
- Second-level breakdowns are designated as (1), (2), (3), etc., as in the past.
- Third-level breakdowns are now designated as (-a), (-b), (-c), etc.
- Fourth-level breakdowns are now designated as (-1), (-2), (-3), etc.
- Fifth-level breakdowns are now designated as (+a), (+b), (+c), etc.
- Sixth-level breakdowns are now designated as (+1), (+2), etc.

Footnotes

With the exception of those included in the front matter (roman-numbered pages), all footnotes are treated as endnotes. The endnotes are referenced in numeric order and appear at the end of each BPVC section/subsection.

Submittal of Technical Inquiries to the Boiler and Pressure Vessel Standards Committees

Submittal of Technical Inquiries to the Boiler and Pressure Vessel Standards Committees has been moved to the front matter. This information now appears in all Boiler Code Sections (except for Code Case books).

Cross-References

It is our intention to establish cross-reference link functionality in the current edition and moving forward. To facilitate this, cross-reference style has changed. Cross-references within a subsection or subarticle will not include the designator/identifier of that subsection/subarticle. Examples follow:

- *(Sub-)Paragraph Cross-References.* The cross-references to subparagraph breakdowns will follow the hierarchy of the designators under which the breakdown appears.
 - If subparagraph (-a) appears in X.1(c)(1) and is referenced in X.1(c)(1), it will be referenced as (-a).
 - If subparagraph (-a) appears in X.1(c)(1) but is referenced in X.1(c)(2), it will be referenced as (1)(-a).
 - If subparagraph (-a) appears in X.1(c)(1) but is referenced in X.1(e)(1), it will be referenced as (c)(1)(-a).
 - If subparagraph (-a) appears in X.1(c)(1) but is referenced in X.2(c)(2), it will be referenced as X.1(c)(1)(-a).
- *Equation Cross-References.* The cross-references to equations will follow the same logic. For example, if eq. (1) appears in X.1(a)(1) but is referenced in X.1(b), it will be referenced as eq. (a)(1)(1). If eq. (1) appears in X.1(a)(1) but is referenced in a different subsection/subarticle/paragraph, it will be referenced as eq. X.1(a)(1)(1).

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ARTICLE RIM-1

SCOPE AND RESPONSIBILITY

RIM-1.1 SCOPE

(a) This Division provides the requirements for the creation of the Reliability and Integrity Management (RIM) Program for all types of nuclear power plants.

(b) The RIM Program addresses a plant's entire life cycle. It is applicable over the entire life of the plant and each passive Structure, System, and Component (SSC) that is in scope. It requires a combination of monitoring, examination, tests, operation, and maintenance requirements that ensure SSCs meet the plant risk and reliability goals (i.e., Reliability Targets) that are selected for the RIM Program. The RIM process consists of the following steps:

- (1) RIM Program scope definition
- (2) degradation mechanism assessment
- (3) plant and SSC Reliability Target allocations originating from the probabilistic risk assessment (PRA)
- (4) identification and evaluation of RIM strategies
- (5) evaluation of uncertainties
- (6) RIM Program implementation
- (7) performance monitoring and RIM Program updates

(c) This Division identifies the areas subject to inspection, monitoring, responsibilities, provisions for accessibility and inspectability, examination methods and procedures, personnel qualifications, frequency of inspection, record keeping and report requirements, procedures for evaluation of inspection and monitoring results and subsequent disposition of results of evaluations, and repair/replacement activity requirements, including procurement, design, welding, brazing, defect removal, fabrication, installation, examination, and leak testing.

RIM-1.2 JURISDICTION

The Owner is responsible for meeting the requirements of Division 1, IWA-1200. In addition, the Owner is responsible for establishing and meeting the Reliability Targets for all SSCs within the scope of this Division.

RIM-1.3 COMPONENTS SUBJECT TO THE REQUIREMENTS OF THIS DIVISION

(a) The RIM Program requirements of this Division shall apply to all SSCs included in the RIM Program scope definition.

(b) SSCs identified in this Division for inspection and monitoring shall be included in the inservice inspection plan. These SSCs include items such as vessels, containments, piping systems, pumps, valves, core support structures, turbine and compressor casings, and storage tanks, including their respective supports.

RIM-1.4 OWNER'S RESPONSIBILITY

The Owner's responsibilities shall include the following:

(a) establishing the Code Editions, Addenda, and Code Cases to be used in Design Specifications and determining that they are acceptable to the regulatory and enforcement authorities having jurisdiction at the nuclear power plant site.

(b) preparation of preservice and inservice plans, schedules, and RIM Program summary reports.

(c) preparation of written examination instructions and procedures, including diagrams or system drawings identifying the extent of areas of components subject to examination.

(d) possession of an arrangement with an Authorized Inspection Agency, recognized by the ASME or national regulatory authorities used to provide inspection services.

(e) establishing a Monitoring and NDE (MANDE) qualification program in accordance with [Mandatory Appendix IV](#).

(f) establishing a RIM Expert Panel (RIMEP) in accordance with [Mandatory Appendix VI](#) responsible for overseeing the RIM Program development and implementation in accordance with [Article RIM-2](#), and the performance of the evaluations for Alternative Requirements in accordance with [Nonmandatory Appendix A](#), if applicable.

(g) establishing a Monitoring and NDE Expert Panel (MANDEEP) responsible for overseeing the qualification of MANDE methods and techniques in accordance with [Mandatory Appendix IV](#), under the RIM Program.

(h) recording MANDE and test results that provide a basis for evaluation and to facilitate comparison with the results of subsequent, MANDE and test activities.

(i) evaluation of MANDE and test results.

(j) performance of repair/replacement activities in accordance with written programs and plans.

(k) maintenance of MANDE, test, flaw evaluation, and repair/replacement activity records, such as radiographs, diagrams, drawings, calculations, MANDE and test data,

description of procedures used, and evidence of personnel qualifications.

- (l) performance of required MANDE and tests.
- (m) retention of MANDE, test, repair/replacement activity records, and flaw evaluation calculations for the service lifetime of the SSCs.
- (n) retention and maintenance of basic calibration blocks and standards used for MANDE and tests of SSCs.
- (o) documentation of a Quality Assurance Program in accordance with ASME NQA-1.
- (p) recording of regions in components where flaws or relevant conditions exceeding the acceptance standards have been evaluated by analysis to allow continued operation. Any continued operation time or cycle limits inherent in the analysis shall also be recorded.
- (q) recording of regions in ferritic steel components where acceptance standards have been modified by the applicable article of [Mandatory Appendix VII](#).
- (r) establishing Reliability Target values for SSCs within the scope of this Division.
- (s) methods other than written signature may be used for indicating certification, authorization, and approval of records; controls and safeguards shall be provided and described in the Quality Assurance Program to ensure the integrity of the certification, authorization, and approval.
- (t) development of analytical evaluation procedures.

RIM-1.5 STANDARD UNITS

The requirements of Division 1, IWA-1700 shall apply.

RIM-1.6 INSPECTION

(21) RIM-1.6.1 Duties of the Inspector and Authorized Nuclear Inservice Inspector Supervisor

- (a) The duties of the Authorized Nuclear Inservice Inspector Supervisor shall be conducted in accordance with the requirements of ASME QAI-1.
- (b) The duties of the Inspector shall be conducted in accordance with ASME QAI-1 and shall include but not be limited to (c) through (l).
- (c) The Inspector shall review the inspection plan and the implementation schedule prior to the start of preservice inspection and each inspection interval and as necessary as a result of any revisions. The review shall cover any features that are affected by the requirements of this Division, as applicable, and shall include the following:
 - (1) examination categories and items
 - (2) MANDE requirements
 - (3) MANDE methods
 - (4) SSCs selected for MANDE and tests
 - (5) disposition of MANDE and test results
 - (6) test frequency
 - (7) system leakage tests
 - (8) sequence of successive MANDE

Shop preservice examinations [\[RIM-2.7.3\(c\)\]](#) are exempt from prior review by the Inspector.

- (d) The Inspector shall review any revisions to the inspection plan and, as necessary, the implementation schedule during the preservice inspection or the inservice inspection interval.
- (e) The Inspector shall submit a report to the Owner documenting review of the items identified in (a) and (b).
- (f) The Inspector shall verify that the RIM Program examinations and leak tests have been performed and the results recorded.
- (g) The Inspector shall perform any additional investigations necessary to verify that the applicable requirements of [RIM-1.6.1](#) have been met.
- (h) The Inspector shall verify that the nondestructive examination methods used follow the techniques specified in this Division and that MANDE activities and tests are performed in accordance with written qualified procedures and by personnel employed by the Owner or the Owner's agent and qualified in accordance with [Mandatory Appendix IV](#).
- (i) The Inspector may require at any time requalification of any procedure or operator if the Inspector has reason to believe that the requirements of this Division are not being met.
- (j) The Inspector shall certify the MANDE and test records after verifying that the requirements of this Division have been met and that the records are correct.
- (k) The Inspector shall verify that repair/replacement activities are performed in accordance with the requirements of the Owner's Repair/Replacement Program.
- (l) The Inspector shall review the Repair/Replacement Program and its implementation.

RIM-1.6.2 Qualification of Authorized Inspection Agencies, Inspectors, and Supervisors

The requirement of Division 1, IWA-2120 shall apply.

RIM-1.6.3 Access for Inspector

The requirement of Division 1, IWA-2130 shall apply.

RIM-1.7 REGULATORY REVIEW

Regulatory bodies may adopt the provisions of [Nonmandatory Appendix B](#) for reporting requirements established by this Division.

RIM-1.8 TOLERANCES

The requirements of Division 1, IWA-1800 shall apply.

RIM-1.9 REFERENCED STANDARDS AND SPECIFICATIONS

When standards and specifications are referenced in this Division, their revision date or indicator shall be as shown in [Table RIM-1.9-1](#).

Table RIM-1.9-1 Referenced Standards and Specifications

Standard, Method, or Specification	Revision Date or Indicator
ANSI/ASNT CP-189	2006
ASME ANDE-1	2015
ASME NQA-1	1994, 2008 through 2015
ASME QAI-1	Latest edition
ASME/ANS RA-S-1.4	Latest edition

ARTICLE RIM-2

RELIABILITY AND INTEGRITY MANAGEMENT (RIM) PROGRAM

RIM-2.1 RIM PROGRAM OVERVIEW

(21) RIM-2.1.1 Basis, Objective, and Process

(a) The reliability of a nuclear power plant and its SSCs is determined by the design, fabrication, inspection, monitoring, operation, and maintenance procedures used to build and operate the plant and its SSCs. Each of these aspects contributes in varying degrees to the reliability of the plant's SSCs. In order for a nuclear power plant to have a level of reliability that will satisfy safety goals, an appropriate combination of these contributors to reliability must be identified and implemented. The objective of the RIM Program is to define, evaluate, and implement strategies to ensure that Reliability Targets for SSCs are defined, achieved, and maintained throughout the plant lifetime.

(b) This Division defines the required elements of the RIM Program for all types of nuclear reactor plants and provides requirements for RIM Program implementation.

(c) The RIM Program shall select the combination of inspection, monitoring, operation, examinations, tests and maintenance requirements that enable the SSCs to meet its Reliability Target in an efficient and cost effective manner.

(d) The process of implementing a RIM Program is illustrated in [Mandatory Appendix I, Figures I-1.1-1 through I-1.1-6](#) and shall include the following process steps:

- (1) RIM Program scope definition
- (2) degradation mechanism assessment
- (3) plant and SSC Reliability Target allocation originating from the probabilistic risk assessment (PRA)
- (4) identification and evaluation of RIM strategies
- (5) evaluation of uncertainties
- (6) RIM Program implementation
- (7) performance monitoring and RIM Program updates

RIM-2.1.2 Responsibilities

RIM-2.1.2.1 Owner's RIM Expert Panel (RIMEP). The RIMEP is responsible for the technical oversight and direction of the risk-informed aspects of RIM Program development and implementation.

RIM-2.1.2.2 RIMEP Qualifications. The requirements of [Mandatory Appendix VI, VI-1.1](#) shall apply.

RIM-2.2 RIM PROGRAM SCOPE AND DEFINITION

The Owner shall document the specific list of SSCs to be evaluated for inclusion within the scope of the RIM Program. The scope shall include SSCs whose failure could adversely affect plant safety and reliability. The Owner shall also document the basis for the exclusion of any SSC considered to be outside the scope of the RIM Program.

RIM-2.3 DEGRADATION MECHANISM ASSESSMENT (DMA)

The potential active degradation mechanisms for the SSCs within the RIM Program scope shall be identified and evaluated.

(a) The following conditions shall be considered in the DMA:

(1) design characteristics, including material, pipe size and schedule, component type (e.g., standard fittings, elbows, flanges), and other attributes related to the system configuration

(2) fabrication practices, including welding and heat treatment

(3) operating and transient conditions, including temperatures, pressures, quality of primary and secondary fluid, and service environment (e.g., humidity, radiation)

(4) plant-specific, industry-wide service experience and research experience

(5) results of preservice, inservice, and augmented examinations and the presence and impact of prior repairs in the system

(6) applicable degradation mechanisms, including those identified in [Mandatory Appendix VII](#) for the applicable plant type

(7) recommendations by SSC vendors for examination, maintenance, repair, and replacement

(b) The criteria used to identify and evaluate the susceptibility of each SSC to degradation mechanisms shall be specified in the RIM Program documentation. The screening criteria found in [Mandatory Appendix VII](#) are minimum requirements to be considered but may be augmented by the RIMEP.

RIM-2.4 PLANT AND SSC RELIABILITY TARGET ALLOCATION

RIM-2.4.1 Plant-Level Risk and Reliability Targets

(a) The RIMEP shall identify plant level risk and Reliability Targets for RIM. Plant level reliability shall be derived from regulatory limits on the risks, frequencies, and radiological consequences of licensing basis events that are defined in the probabilistic risk assessment (PRA).

The RIM Program may be developed for single reactor module or plants with two or more reactor modules. Event sequence frequencies shall be expressed in terms of events per plant year where the plant may include a single reactor or multiple reactor modules. The event sequence consequences may involve source terms from single or multiple reactor modules, or source terms from non-core related radionuclide sources and associated off-site radiological consequences.

(b) Plant level RIM goals may include additional goals to meet plant availability.

RIM-2.4.2 SSC-Level Reliability Target

(a) The RIMEP shall use information provided by the plant specific PRA to identify SSC-level Reliability Targets for SSCs relied upon to prevent and mitigate the consequences of accident scenarios and in a manner that is consistent with the plant level reliability goals.

(b) The PRA model shall be used to allocate SSC Reliability Targets from and consistent with the plant level reliability goals.

(c) The allocation of SSC-level Reliability Targets shall consider the uncertainties inherent in the prediction of SSC reliability.

(d) SSC-level Reliability Targets may also be identified by the RIMEP for overall plant availability considerations.

(e) The methodology for deriving Reliability Targets is contained in [Mandatory Appendix II](#).

RIM-2.4.3 Scope, Level of Detail, and Technical Adequacy of the PRA

(a) The scope of the PRA used to allocate SSC Reliability Targets shall address

(1) the plant operating states relevant to the plant level risk and reliability goals and SSC-level Reliability Targets

(2) a full set of initiating events including internal events and events associated with external plant hazards

(3) event sequence development that is sufficient to support the quantification of mechanistic source terms and offsite radiological consequences consistent with applicable regulatory limits on the frequencies and consequences of accident scenarios

Although all plant operating modes and hazard groups shall be addressed, it is not always necessary to have a full-scope PRA as outlined above. Qualitative treatment or

other risk information related to missing modes and hazard groups may be sufficient if it can be demonstrated that those risk contributions would not affect the Reliability Targets or other aspects of the RIM Program.

(b) The level of detail required of the PRA is that which is sufficient to establish Reliability Targets for the SSCs to be included in the RIM Program. If the SSCs of interest cannot be associated with elements of the PRA, the PRA should be modified accordingly.

PRA models for current light water reactor (LWR) types frequently exclude passive components (e.g. piping) due to their much lower failure probabilities than active components. For implementation of RIM and the allocation of Reliability Targets, such components would need to be included in the PRA if included within the scope of the RIM Program.

(c) Technical adequacy refers to the suitability of the PRA modeling and the reasonableness of the underlying assumptions and approximations. The PRA shall meet the requirements of the ASME/ANS RA-S-1.4, Probabilistic Risk Assessment Standard for Advanced Non-LWR for Nuclear Power Plants, latest edition, to the extent necessary to support RIM Program development. The PRA standard provides technical supporting requirements in terms of Capability Categories. The delineation of Capability Categories is such that the PRA scope, level of detail, plant specificity and realism increase from Capability Category I to Capability Category II. Current good practice (Capability Category II) is generally expected to be necessary to support RIM, although Capability Category I may be sufficient for some requirements. All significant PRA peer review findings shall be reviewed and dispositioned by incorporating changes into the PRA model, performing sensitivity studies to evaluate the identified issue, or providing justification for the original PRA model. The results of the PRA peer review and the review of other risk information used in the RIM Program development shall be documented in a characterization of the adequacy of the PRA.

NOTE: ASME/ANS RA-S, Standard for Level 1/Large Early Release Frequency Probabilistic Risk Assessment for Nuclear Power Plant Applications, shall be used for current technology BWR and PWR light water reactor (LWR) designs, and ASME/ANS RA-S-1.5, Advanced Light Water Reactor PRA Standard (currently in development), shall be used for Advanced LWR technology.

RIM-2.5 IDENTIFICATION AND EVALUATION OF RIM STRATEGIES

The RIMEP shall identify the RIM strategies that are available to meet the Reliability Targets and evaluate and select combinations of strategies that will meet and maintain the Reliability Targets.

RIM-2.5.1 Identification of RIM Strategies

(a) The strategies shall account for all factors that contribute to reliability. These factors shall include but not necessarily be limited to

- (1) design strategies, including material selection
- (2) fabrication procedures
- (3) operating practices
- (4) preservice and inservice examinations
- (5) testing
- (6) MANDE
- (7) maintenance, repair, and replacement practices

(b) The evaluated RIM strategies shall account for the potential for specific degradation mechanisms applicable to each SSC in the scope of the RIM Program identified in [Mandatory Appendix VII](#).

(c) The RIMEP shall select the RIM strategies or combinations of strategies that are necessary and sufficient to achieve and maintain SSC reliability consistent with SSC Reliability Targets established in [RIM-2.4.2](#).

(d) In addition to use of probabilistic methods that are permitted by this Division for establishing MANDE criteria, deterministic methodology for examinations and acceptance criteria, as outlined in [Nonmandatory Appendix A, A-3.5](#) may be used.

RIM-2.5.2 Evaluation of RIM Strategy Impacts on SSC Reliability

(a) The impact of each RIM strategy that is considered for inclusion into the RIM Program in accordance with [RIM-2.5](#) on the reliability of each SSC in the scope of the RIM Program shall be assessed for comparison against the SSC-level Reliability Targets. This assessment shall include

(1) application of acceptable SSC reliability assessment methods, such as statistical analysis of failure data, probabilistic fracture mechanics, Markov modeling, expert elicitation, or appropriate combinations of these methods.

(2) assessment of SSC plant specific failure rates that correspond to the frequencies of initiating events and PRA and SSC failure probabilities for mitigating events in the PRA model. This formulation shall be consistent with the reliability metrics selected for the SSC Reliability Target allocation in accordance with [RIM-2.4.2](#).

(3) evaluation of the effectiveness of the RIM strategy that accounts for the quantity and applicability of applied failure data, uncertainty in the estimates of component exposure populations, materials, variability of operating conditions, and variability of expert opinion.

(4) identification and evaluation of the effectiveness and extent of the RIM strategy or combination of strategies including the percentage of the SSCs to which the strategy is applied, probability of detection, inspection frequency, flaw sizing accuracy, time to detect, accessibility, and other

factors of the RIM Program that influence the SSC reliability.

RIM-2.6 EVALUATION OF UNCERTAINTIES

The RIMEP shall identify additional RIM strategies over and above those determined in accordance with [RIM-2.5](#) that are necessary to provide additional assurance that the Reliability Targets will be achieved and maintained during the SSC service lifetime in order to address uncertainties in predicting SSC reliability performance. Specific RIM strategies that are included to address these uncertainties shall be documented in accordance with [RIM-2.7.1](#).

RIM-2.7 RIM PROGRAM IMPLEMENTATION

RIM-2.7.1 RIM Program Documentation

(a) The Owner shall document the RIM strategies that are selected for inclusion into the RIM Program as part of the RIM Program documentation. This documentation shall include the following:

- (1) the scope of SSCs selected for inclusion in the RIM Program
- (2) the results of the DMA evaluation for the SSCs in the RIM Program
- (3) the plant level risk and reliability goals
- (4) SSC Reliability Targets derived from the plant level risk and reliability goals
- (5) technical adequacy of the PRA and risk information used to derive the SSC Reliability Target
- (6) the specific RIM strategies selected for the RIM Program for each SSC including associated performance parameters that are required to achieve Reliability Targets, (e.g., probability of detection, inspection intervals)
- (7) the evaluation of the impact of RIM strategies and combination of RIM strategies on the SSC reliability performance
- (8) the quantification of uncertainties and evaluation of additional RIM strategies selected to address uncertainties

(b) The RIM Program documentation shall be updated periodically to evaluate changes to any of the technical inputs as described in [RIM-2.8](#), but no later than the end of each established inspection interval.

RIM-2.7.2 Inspection Interval

(a) Inservice examinations selected for inclusion into the RIM Program for specific SSCs shall be completed during each inspection interval for the service lifetime of the plant. The inspections shall be performed in accordance with the schedule for implementing the RIM Program.

(b) The inspection interval shall be determined by the RIMEP and shall not exceed 12 yr.

(c) The interval shall be divided into two or more approximately equal inspection periods for planning the examinations over the inspection interval. The examinations that are required for each interval shall be approximately equally distributed over the inspection periods.

(d) Each inspection interval may be reduced or extended by as much as 1 yr. Adjustments shall not cause successive intervals to be altered by more than 1 yr from the original pattern of intervals. If an inspection interval is extended, neither the start and end dates nor the RIM Program for the successive interval need be revised.

(e) Examinations may be performed to satisfy the requirements of the extended interval in conjunction with examinations performed to satisfy the requirements of the successive interval. However, an examination performed to satisfy requirements of either the extended interval or the successive interval shall not be credited to both intervals.

(f) That portion of an inspection interval described as an inspection period may be reduced or extended by as much as 1 yr to enable an inspection to coincide with a plant outage. This adjustment shall not alter the requirements for scheduling inspection intervals.

(g) The inspection interval for which an examination was performed shall be identified on examination records.

(h) In addition to (d), for plants that are out of service continuously for 6 months or more, the inspection interval during which the outage occurred may be extended for an inspection period equivalent to the outage and the original pattern of intervals extended accordingly for successive intervals.

(i) The inspection intervals for items installed by repair/replacement activities shall coincide with remaining intervals, as determined by the calendar years of plant service at the time of the repair/replacement activities.

RIM-2.7.3 Preservice Inspection

(a) For those categories of SSCs for which examinations have been selected as a RIM strategy for inclusion in the RIM Program, a preservice examination shall be performed. If any percentage of the SSC category has been selected for inservice examination, then 100% of the SSCs shall be subjected to a preservice examination using the same examination method used for inservice examination. The purpose of these preservice examinations is to establish a baseline in the event an inservice examination is required at each location. These preservice baseline examinations shall be performed using personnel, procedures and equipment that have been qualified and demonstrated to the Inspector to reliably detect and accurately characterize fabrication flaws. These examinations shall be documented using encoded equipment and scanners, (no manual examinations allowed), and a

permanent archival record of the flaws identified shall be created for material examined. The examination records and results shall be reviewed by the Inspector to ensure that potential flaws are assessed and completeness of records is established. Flaws identified in these examinations shall be evaluated for service in accordance with the flaw acceptance criteria in [Article RIM-3](#). Selection of the analytical evaluation method is the responsibility of the MANDEEP.

(b) The examinations required by this Article for those components initially selected for examination in accordance with the RIM Program shall be completed prior to initial plant startup.

(c) Shop and field examinations may serve in lieu of the on-site preservice examinations, provided

(1) in the case of vessels only, the hydrostatic test required by the Construction Code has been completed

(2) such examinations are conducted and meet the requirements under (a)

(3) the shop and field examination records are, or can be, documented and identified in a form consistent with those required in [Article RIM-6](#)

RIM-2.7.4 Design Requirements for RIM

(a) The RIM Program shall consider the design requirements of SSCs that are identified as part of the RIM strategies established in [RIM-2.5](#) and as may be required to prevent or reduce the susceptibility to degradation mechanisms determined in [RIM-2.3](#) or otherwise needed to support a selected RIM strategy, e.g., provision for an online leak detection system.

(b) The design requirements that result from any plant modifications to an SSC within the scope of the RIM Program shall include considerations to assure that adequate access is maintained in order to be able to perform MANDE over the life of the SSC(s).

RIM-2.7.5 Leak Detection System Requirements for RIM

The leak detection capabilities of monitoring systems that are employed as a selected RIM strategy shall have performance characteristics such as probability of detection, time to detect, minimum detectable leak rate, and system reliability and availability characteristics that are sufficient to meet SSC RIM Reliability Targets established in [RIM-2.4.2](#). Verification of adequate performance of online leak detection systems shall be demonstrated in accordance with [RIM-5.2](#).

RIM-2.7.6 Examination and Inspection Requirements for RIM

RIM-2.7.6.1 General Monitoring and Examination Requirements

(a) MANDE criteria shall be defined so the scope, method, detection reliability, frequency, and performance demonstration provides information to demonstrate that the Reliability Targets continues to be met for the SSCs included in the RIM Program as established in [RIM-2.4.2](#).

(b) MANDE performed to provide and maintain SSC Reliability Targets shall meet, where applicable, the following requirements:

(1) The functional or structural reliability of a system or system components shall be monitored using a program that may include one or more of the following activities that could be done either periodically or continuously:

- (-a) operating fluid leakage detection and monitoring
- (-b) monitoring the amount of make-up fluid
- (-c) walk downs to monitor the operating fluid level in storage tanks
- (-d) monitoring fluid level or flow in drains
- (-e) monitoring humidity levels
- (-f) monitoring radiation levels
- (-g) auxiliary operator plant walk-through

(2) MANDE activities shall be conducted on any SSC within the RIM Program scope. It may include: continuous leakage monitoring or periodic leak testing as required to meet the allocated SSC Reliability Target.

(3) The functional or structural reliability of a system or system components shall be monitored using a program that considers the following factors:

- (-a) potential for active degradation mechanisms
- (-b) radiological consequences of SSC failure
- (-c) personnel radiation exposure
- (-d) insights from plant and industry service or research experience

(c) MANDE requirements for the SSCs within the scope of the RIM Program for which specific requirements have not been specified shall be defined by the RIMEP and documented with a technical basis.

(d) The MANDE methods and procedures shall account for the potential degradation mechanisms identified in [Mandatory Appendix VII](#).

(e) Examination volumes, methods, and frequencies appropriate for each degradation mechanism are provided in [RIM-2.7.7](#) and [Mandatory Appendix V](#) and augmented for specific reactor designs as outlined in the relevant reactor design article contained in [Mandatory Appendix VII](#).

RIM-2.7.6.2 Examination Locations. The location and number of NDE examinations shall be defined using the following requirements in each inspection interval:

(a) The minimum number of locations shall be selected to meet the SSC Reliability Target.

(b) Examination locations shall be selected in accordance with the following criteria:

(1) Locations where the consequence of a postulated rupture would result in high risk.

(2) To maintain personnel exposure within acceptable limits, examinations generally will be performed away from areas with high irradiation levels.

(3) Locations where 100% of the areas of concern can be examined.

RIM-2.7.6.3 Successive Examinations

(a) If an SSC is accepted for continued service in accordance with [Article RIM-3](#), the areas containing flaws or relevant conditions shall be reexamined based on the MANDE and periodicity criteria established by the flaw evaluation results.

(b) If the reexaminations required by (a) reveal that the flaw or relevant condition remain essentially unchanged, the SSC MANDE schedule may revert to the original schedule of successive inspections.

RIM-2.7.6.4 Additional Examinations

(a) Examinations performed in accordance with [Mandatory Appendix V](#) and any augmented provisions from [Mandatory Appendix VII](#) supplements applicable to a specific reactor design, that reveal a flaw or a relevant condition exceeding the acceptance standards of [Mandatory Appendix VII](#), [Table VII-1.3.3-1](#) or [Table VII-3.3.3-1](#) shall be extended to include additional examinations during the current outage. The additional examinations shall include an additional number of welds, areas of interest, or parts and shall be determined by and the basis documented by MANDEEP. The additional examinations shall be selected from welds, areas of interests, or parts of similar material and service. This additional selection may require inclusion of SSCs other than the one containing the flaws or relevant conditions.

(b) If the additional examinations required by (a) reveal a flaw or a relevant condition exceeding the acceptance standards of [Mandatory Appendix VII](#), [Table VII-1.3.3-1](#) or [Table VII-3.3.3-1](#), the examinations shall be further extended to include additional examinations during the current outage. These additional examinations shall include the remaining welds, areas of interest, or parts of similar material and service subject to the same type of flaws or relevant conditions.

(c) For the inspection period following the period in which the examinations of (a) or (b) were completed, the examinations shall be performed as originally scheduled.

(d) No additional examinations are required if either of the following applies:

(1) There are no other SSC subject to the same apparent or root cause conditions.

- (2) The degradation mechanism no longer exists.

RIM-2.7.7 Examination Methods and Volumes

(a) Examination programs developed in accordance with [Article RIM-2](#) shall use examination techniques suitable for specific degradation mechanisms and examination locations. The examination volumes and methods that shall be considered by MANDEEP in establishing MANDE criteria, and that are applicable to each degradation mechanism, are provided in the applicable article of [Mandatory Appendix VII](#) and [Mandatory Appendix V](#).

(b) The personnel, equipment, and procedures used for the examinations shall be qualified to reliably detect and size the relevant degradation identified for each element in accordance with [Mandatory Appendix IV](#). Examinations shall be conducted and documented in accordance with [RIM-2.8](#).

RIM-2.8 PERFORMANCE MONITORING AND RIM PROGRAM UPDATES

(a) The affected portions of the RIM Program shall be reevaluated to incorporate results from SSC performance MANDE and new information affecting implementation of the program as it becomes available. New information may include the following:

(1) changes to plant design, which may introduce (or remove) SSCs within the scope of the RIM Program, as well as changes in materials, configurations, stresses, etc. Changes to plant design may also result in significant changes to plant risk, as determined by PRA update, which may require update of the Reliability Target allocations.

(2) changes to plant procedures, such as operating parameters, system lineups, equipment, and operating modes, may result in different degradation mechanisms or MANDE capability, as well as changes to plant risk, as determined by PRA update.

(3) changes in SSC performance, indicating a potential change in reliability.

(4) MANDE results that indicate service-related degradation.

(5) Industry or research experience, including SSC failure or reliability data or degradation mechanisms.

(b) RIM Program updates may include adjustment of SSC Reliability Targets based on new information described in (a) and/or PRA updates.

(1) Reliability Targets should not be decreased to correspond with changes in SSC performance or service-related degradation, without determining the risk impact and the effect on other Reliability Target allocations based on the derivation methodology in [Mandatory Appendix II](#) and additional considerations in [RIM-2.10](#).

(2) The minimum frequency of RIM Program updates shall be at each inspection interval as specified in [RIM-2.7.2\(b\)](#). RIM Program updates should be more frequent if dictated by PRA updates or if new degradation mechanisms are identified.

RIM-2.9 EXAMINATION METHODS

RIM-2.9.1 Visual Examinations

Visual examinations shall be conducted in accordance with Section V, Article 9; Division 1, Table IWA-2211-1; and the following requirements:

(a) A written procedure and report of examination results are required.

(b) For procedure demonstration, a test chart containing text with some lowercase characters without an ascender or descender (e.g., a, c, e, o) meeting Division 1, Table IWA-2211-1 is required. Measurements of the test chart shall be made once before initial use with an optical comparator (10X or greater) or other suitable instrument to verify that the height of a representative lower case character without an ascender or descender, for the selected type size, meets the requirements of Division 1, Table IWA-2211-1.

(c) Remote examination may be substituted for direct examination. The remote examination procedure shall be demonstrated to resolve the selected test chart characters.

(d) Alternatives to the direct visual examination distance requirements of Section V may be used as specified in Division 1, Table IWA-2211-1.

(e) It is not necessary to measure illumination levels on each examination surface when the same portable light source or similar installed lighting equipment is demonstrated to provide the illumination specified in Division 1, Table IWA-2211-1 at the maximum examination distance.

(f) The adequacy of the illumination levels from battery powered portable lights shall be checked before and after each examination or series of examinations, not to exceed 4 hours between checks. In lieu of using a light meter, these checks may be made by verifying that the illumination is adequate (i.e., no discernable degradation in the visual examination resolution of the procedure demonstration test chart characters).

RIM-2.9.1.1 VT-1 Examination. VT-1 examination is conducted to detect discontinuities and imperfections on the surface of components, including such conditions as cracks, wear, corrosion, or erosion.

RIM-2.9.1.2 VT-2 Examination. VT-2 examination is conducted to detect evidence of leakage from a pressure-retaining component after a repair/replacement activity. The examination shall be conducted in accordance with [Article RIM-5](#).

RIM-2.9.1.3 VT-3 Examination. VT-3 examination is conducted to determine the general mechanical and structural condition of components and their supports by verifying parameters such as clearances, settings, and physical displacements; to detect discontinuities and imperfections, such as loss of integrity at bolted or welded connections, loose or missing parts, debris, corrosion, wear, or erosion; and to detect conditions that could affect operability or functional adequacy of constant load and spring-type supports.

RIM-2.9.1.4 Surface Replication. Surface replication methods may be used for VT-1 and VT-3 examinations when the surface resolution is at least equivalent to that of direct visual observation. The personnel that will evaluate the surface replication will be qualified in accordance with [Mandatory Appendix IV](#).

RIM-2.9.1.5 Remote Visual Examination. In addition to the requirements of Section V, Article 9, when remote visual examination is substituted for direct visual examination, the remote visual examination system shall have the capability of distinguishing and differentiating between the colors applicable to the requirements of VT-1 and VT-3 for the component examinations being conducted.

RIM-2.9.2 Surface Examination

(a) A surface examination may be conducted using a magnetic particle, liquid penetrant, eddy current, or ultrasonic method.

(b) Any linear indication detected by magnetic particle, liquid penetrant, or eddy current examination that exceeds the allowable linear surface flaw standards shall be recorded.

(c) Any flaw recorded by ultrasonic examination shall be compared to the volumetric examination acceptance standards of [Mandatory Appendix VII](#), [VII-1.4.3](#) or [VII-3.4.3](#) for allowable planar or linear flaws.

RIM-2.9.2.1 Magnetic Particle Examination

(a) Magnetic particle examination shall be conducted in accordance with Section V, Article 7.

(b) Magnetic particle examination of coated materials shall be conducted in accordance with Section V, Article 7.

RIM-2.9.2.2 Liquid Penetrant Examination. Liquid penetrant examination shall be conducted in accordance with Section V, Article 6.

RIM-2.9.2.3 Eddy Current Examination. Eddy current examination for detection of surface flaws shall be conducted in accordance with Division 1, Mandatory Appendix IV.

RIM-2.9.2.4 Ultrasonic Examination. An ultrasonic examination performed from the inside surface of piping may be used as a surface examination method

for piping welds NPS 4 (DN 100) and larger. The ultrasonic examination technique shall be demonstrated capable of detecting an acceptable flaw having the greatest a/t ratio or a 0.50 aspect ratio at the surface being examined.

RIM-2.9.3 Volumetric Examination

A volumetric examination may be conducted from either the inside or outside surface of a component.

RIM-2.9.3.1 Radiographic Examination. Radiographic examinations employing either X-ray equipment or radioactive isotopes shall be conducted in accordance with Section V, Article 2.

RIM-2.9.3.2 Ultrasonic Examination. Ultrasonic examination shall be conducted in accordance with Division 1, Mandatory Appendix I.

RIM-2.9.3.3 Eddy Current Examination. Eddy current examination shall be conducted in accordance with Section V, Article 8.

RIM-2.9.3.4 Acoustic Emission Monitoring and Examination. Acoustic emission may be used in lieu of the successive inspections of [RIM-2.7.6.3](#) to monitor growth of flaws detected by other NDE methods. The flaws shall be sized by ultrasonic examination in accordance with Division 1, Mandatory Appendix I, prior to initiating use of acoustic emission. Acoustic emission monitoring shall be initiated prior to resuming operation of the system. Acoustic emission shall be conducted in accordance with Section V, Article 13, with the following additional requirements:

(a) The following flaw growth calculation and acceptance criteria shall be used:

(1) Every 2 months during the current inspection period, calculate the flaw growth in accordance with Section V, Article 13. Using this growth rate, predict the flaw size at the end of the current inspection period.

(2) If the calculated flaw size at the end of the current inspection period meets the acceptance criteria of [Mandatory Appendix VII](#), [VII-1.5](#) or [VII-3.5](#), as applicable, continue the 2-month monitoring process described in (1) above.

(3) If the calculated flaw size at the end of the current inspection period does not meet the acceptance criteria of [Mandatory Appendix VII](#), [VII-1.5](#) or [VII-3.5](#), as applicable, the following actions shall be performed:

(-a) Calculate the flaw size at the end of the next 2-month time span. If this calculated flaw size meets the acceptance criteria of [Mandatory Appendix VII](#), [VII-1.5](#) or [VII-3.5](#), as applicable, continue the 2-month monitoring process described in (1) above.

(-b) If the calculated flaw size at the end of the next 2-month time span does not meet the acceptance criteria of [Mandatory Appendix VII](#), [VII-1.5](#) or [VII-3.5](#), as applicable, the component shall be corrected by repair/

replacement activity in accordance with [Mandatory Appendix VII](#), [VII-1.3.1.3](#) or [VII-3.3.1.3](#), as applicable.

RIM-2.9.4 Alternative Examinations

Alternative examination methods, a combination of methods, or newly developed techniques may be substituted for the methods specified in the Construction Code or this Division, provided any alternate criteria are approved by MANDEEP in accordance with [Mandatory Appendix IV](#) and the Inspector is satisfied that the results are demonstrated to be equivalent or superior to those of the specified method and the basis for this improvement has been fully documented. The methodology for determining alternative examinations may be determined using [Nonmandatory Appendix A](#) criteria.

RIM-2.10 ADDITIONAL CONSIDERATIONS FOR RIM PROGRAM IMPLEMENTATION

RIM-2.10.1 Consequence, External Event, and Shutdown Considerations

(a) Allocation of Reliability Targets using the derivation methodology presented in [Mandatory Appendix II](#) should be performed with a PRA model that includes evaluation of consequences (such as release frequency or dose), as well as contribution from external hazards (flood, fire, seismic, high wind, etc.) and low power and shutdown (LPSD) modes of operation.

(b) If the PRA model does not integrate consequences and risk, the RIMEP must consider if the SSCs included in the RIM Program are involved in the mitigation of consequences and whether the associated Reliability Targets should be adjusted accordingly.

(c) If the PRA model does not include the analysis of certain external hazards, the RIMEP must consider if the SSCs included in the RIM Program are involved in the protection against those external hazards and whether the associated Reliability Targets should be adjusted accordingly. This consideration may be based on qualitative information such as an external hazards screening analysis.

(d) If the PRA model does not include the analysis of LPSD modes, the RIMEP must consider if the SSCs included in the RIM Program are important to LPSD safety and whether the associated Reliability Targets should be adjusted accordingly. This consideration may be based on qualitative information such as a shutdown safety plan.

RIM-2.10.2 Principles of Risk-Informed Decision Making

The RIMEP should ensure the principles of risk-informed decision-making are met when implementing the RIM Program.

(a) The RIM Program shall meet current regulations.

(b) The RIM Program shall be consistent with the philosophy of defense-in-depth. The impact of the RIM Program on the functional capability, reliability, and availability should be assessed for the included SSCs that provide layers of defense to ensure that

(1) a reasonable balance among the layers of defense is preserved

(2) adequate capability of design features is preserved without overreliance on programmatic activities

(3) system redundancy, independence, and diversity is preserved

(4) adequate defense against potential common-cause failures is preserved

(5) multiple fission product barriers are maintained

(6) sufficient defense against human errors is maintained

(7) the intent of the plant's design criteria continues to be met

(c) The RIM Program shall maintain sufficient safety margins such that

(1) the codes and standards approved for use continue to be met

(2) safety analysis acceptance criteria in the licensing basis continue to be met

(d) Risk, including any changes in risk gained from operating experience of an SSC and the impact of uncertainty, should be small and consistent with regulatory requirements.

(1) Evaluation of risk impact might entail the use of quantitative PRA results or bounding risk calculations, or a qualitative assessment may be sufficient depending on the significance of the impact.

(2) The impact of uncertainties, and associated assumptions and approximation, on the risk results should be identified and understood.

(e) The RIM Program shall be monitored using performance measurement strategies (as described in [RIM-2.8](#)), such that

(1) SSC performance monitoring shall be used to demonstrate the performance is consistent with the assumptions in the RIM Program

(2) the rigor of the SSC performance monitoring is commensurate with the safety importance of the SSC

(3) degradation in SSC performance is detected and corrected before plant safety is compromised

ARTICLE RIM-3 ACCEPTANCE STANDARDS

RIM-3.1 EVALUATION OF EXAMINATION RESULTS AND ACCEPTANCE STANDARDS

Flaw acceptance standards for reactor components subjected to various operating environments and constructed to various construction codes may be found in the following articles of [Mandatory Appendix VII](#):

(a) For components in light water reactor-type plants, flaw acceptance standards shall be obtained from [Mandatory Appendix VII, Article VII-1](#).

(b) For components in liquid metal reactor-type plants, flaw acceptance standards shall be obtained from [Mandatory Appendix VII, Article VII-2](#).

(c) For components in helium reactor-type plants, flaw acceptance standards shall be obtained from [Mandatory Appendix VII, Article VII-3](#).

(d) For components in molten salt reactor-type plants, flaw acceptance standards shall be obtained from [Mandatory Appendix VII, Article VII-4](#).

(e) For components in Generation 2 light water reactor-type plants, flaw acceptance standards shall be obtained from the Reactor Type [Mandatory Appendix VII, Article VII-5](#).

(f) For components in fusion machine-type plants, flaw acceptance standards shall be obtained from [Mandatory Appendix VII, Article VII-6](#).

ARTICLE RIM-4

REPAIR/REPLACEMENT ACTIVITIES

(21) RIM-4.1 SCOPE

If an SSC falls within the scope of the RIM Program, repair/replacement activities shall be done in accordance with Division 1, IWA-4000, except for the following:

(a) In lieu of the preservice inspection requirements of Division 1, IWA-4530, the preservice examination requirements of RIM-2.7.3 shall apply.

(b) In lieu of the pressure testing requirements of Division 1, IWA-4540(a), the system leakage requirements of RIM-4.2 shall apply.

(c) For applicable paragraphs that identify more than one Code Class, the activity shall be performed to Class 1 requirements unless otherwise specified in the RIM Program.

RIM-4.2 LEAK TEST REQUIREMENTS AFTER A REPAIR/REPLACEMENT ACTIVITY

Leak testing shall be performed following repair/replacement activities in accordance with the requirements of RIM-4.2.2 or RIM-4.2.3, regardless of the fluid normally contained in the system during operation.

RIM-4.2.1 Test Boundaries

(a) Only the pressure boundary affected by the repair/replacement activity must be tested.

(b) Open ended portions of a non-closed system extending to the first shutoff valve may be exempted from the test requirements.

RIM-4.2.2 Gas Leak Test

(a) *Test Description.* The leak test shall be performed in accordance with Section V, Article 10, Mandatory Appendix IV.

(b) *Test Medium.* The gas used as the test medium shall be nonflammable when a test is made on a gas system.

(c) *Pressure and Temperature*

(1) Leakage tests shall be conducted at normal operating system pressure.

(2) The test pressure shall be verified by normal system instrumentation (such as control room instruments) or test instrumentation.

(3) The test conditions shall be maintained essentially constant during the course of the test.

(4) The test pressure and temperature may be obtained by using any means that comply with the plant Technical Specifications.

(d) *Test Condition Holding Time.* For leak tests, a 10-minute holding time is required after attaining test pressure.

(e) *Visual Examination.* The VT-2 visual examination shall be conducted by examining the accessible external exposed surfaces of pressure-retaining components for evidence of leakage.

RIM-4.2.3 Liquid Leak Test

(a) *Test Description.* The leak test shall be performed in accordance with Section V, Article 10, Mandatory Appendix IV or Mandatory Appendix VI.

(b) *Test Medium.* The contained fluid in the system shall serve as the pressurizing medium.

(c) *Pressure and Temperature*

(1) Leak tests shall be conducted at normal operating system pressure.

(2) The test pressure shall be verified by normal system instrumentation such as control room instruments or test instrumentation.

(3) The test conditions shall be maintained essentially constant during the course of the test.

(4) When portions of a system are subject to system leak tests associated with two different system functions, the visual examination need only be performed during the test conducted at the higher of the test pressures of the respective system function.

(5) The test pressure and temperature may be obtained by using any means that comply with the plant Technical Specifications.

(d) *Test Condition Holding Time*

(1) For leak tests, a 10-minute holding time for non-insulated components, or 4 hours for insulated components, is required after attaining test pressure.

(2) For components not required to operate during normal plant operations, a 10-minute holding time is required after attaining test pressure.

(e) *Visual Examination.* The VT-2 visual examination shall be conducted by examining the accessible external exposed surfaces of pressure-retaining components for evidence of leakage.

RIM-4.2.4 Volumetric and Surface Examination

In lieu of the leak testing requirements of [RIM-4.2.2](#) or [RIM-4.2.3](#), the area affected by the repair/replacement activity may be examined using a volumetric and surface examination method and shall meet the requirements of [Article RIM-3](#). The requirements of [RIM-5.2](#) shall apply.

RIM-4.2.5 Exemptions

The following are exempt from any leak test:

- (a) cladding
- (b) heat exchanger tube plugging and sleeving
- (c) welding or brazing that does not penetrate through the pressure boundary
- (d) flange seating surface when less than half the flange axial thickness is removed and replaced
- (e) tube-to-tubesheet welds when such welds are made on the cladding
- (f) seal welds
- (g) welded or brazed joints between nonpressure-retaining items and the pressure-retaining portion of the components
- (h) valve discs or seats
- (i) bolts, studs, nuts or washers

For additional exemptions, refer to the applicable reactor-type supplement in [Mandatory Appendix VII](#).

RIM-4.3 RESPONSIBILITIES

The Owner shall prepare the Owner's Repair/Replacement Certification Record, Form NIS-2, in accordance with [Mandatory Appendix III](#) upon completion of all required activities associated with the Repair/Replacement Plan necessary to place the item in service.

RIM-4.4 CORRECTIVE ACTION

(a) The sources of leakage detected by a leak test shall be located and evaluated by the Owner for corrective action as follows:

(1) Leaks such as from seals, seats, and gasket joints in components may be permitted when specifically allowed by the Owner's Design Specification.

(2) An evaluation of the effect of any degraded area upon the structural integrity of the pressure boundary shall be performed in accordance with the provisions of [Article RIM-3](#).

(b) Components requiring corrective action shall have repair/replacement activities performed in accordance with [Article RIM-4](#) or corrective measures performed where the relevant condition can be corrected without a repair/replacement activity. All pressure testing required by repair replacement activities shall be completed before returning an SSC to service.

RIM-4.5 RECORDS

The results of the leakage tests performed to complete a repair/replacement activity shall be documented.

ARTICLE RIM-5

SYSTEM LEAK MONITORING AND PERIODIC TESTS

RIM-5.1 SCOPE

This Article provides requirements for leakage monitoring and periodic leak testing of a pressure-retaining system or components.

RIM-5.2 LEAKAGE MONITORING

RIM-5.2.1 General

Systems provided for continuous online leakage monitoring as an element of the RIM Program shall be subjected to the reliability performance requirements of [RIM-2.7.5](#). During plant operation the leakage detection systems shall be in operation. Verification of proper leakage detection system operation and effectiveness shall be made on a daily basis. Verification will include but is not limited to the following:

- (a) system calibration records
- (b) system printouts
- (c) system monitoring
- (d) system maintenance history
- (e) records of performance demonstration tests

RIM-5.2.2 Periodic Leak Test

The requirements of [RIM-4.2.2](#), Gas Leak Test, or [RIM-4.2.3](#), Liquid Leak Test, as applicable, shall be used for the conduct of periodic leak tests.

RIM-5.3 CORRECTIVE ACTION

(a) The sources of leakage detected by leakage monitoring or leak test shall be located and evaluated by the Owner for corrective action as follows:

(1) Leaks such as from seals, seats, and gasket joints in components may be permitted when specifically allowed by the Owner's Design Specification.

(2) An evaluation of the effect of any degraded area upon the structural integrity of the pressure boundary shall be performed in accordance with the provisions of [Article RIM-3](#).

(b) Components requiring corrective action shall have repair/replacement activities performed in accordance with [Article RIM-4](#) or corrective measures performed where the relevant condition can be corrected without a repair/replacement activity.

RIM-5.4 RECORDS

(a) The record of the verification of satisfactory performance of the leakage monitoring system shall be documented. Any source of leakage or evidence of structural distress shall be itemized, and the location and corrective action documented.

(b) The results of periodic leak tests shall be documented as required by [RIM-6.3.4](#).

ARTICLE RIM-6

RECORDS AND REPORTS

RIM-6.1 SCOPE

This Article provides the requirements for the preparation, submittal, and retention of records and reports.

RIM-6.2 REQUIREMENTS

RIM-6.2.1 Owner's Responsibilities

(a) The Owner shall prepare plans and schedules for the RIM Program to meet the requirements of this Division.

(b) The Owner shall prepare records of MANDE results, tests, and repair/replacement activities.

(c) The Owner shall prepare the Owner's Activity Report, Form OAR-1 in [Mandatory Appendix III](#).

(d) The Owner shall prepare the Owner's Repair/Replacement Certification Record, Form NIS-2, in accordance with [Mandatory Appendix III](#) upon completion of the required activities associated with the Repair/Replacement Plan.

RIM-6.2.2 Owner Activity Report, Form OAR-1

An Owner's Activity Report, Form OAR-1 in [Mandatory Appendix III](#), shall be processed as specified below following the completion of each scheduled outage for each single reactor in a facility.

(a) A listing of the items with flaws or relevant conditions that exceeded the acceptance criteria of this Division and that required evaluation to determine acceptability for continued service shall be provided with the information and format of Form OAR-1, Table 1. This information is required whether or not the flaw or relevant condition was discovered during a scheduled examination, test or during MANDE activities.

(b) An abstract for the repair/replacement activities that were required due to an item containing a flaw or relevant condition that exceeded the acceptance criteria of this Division shall be provided with the information and format of Form OAR-1, Table 2. The information is required even if the discovery of the flaw or relevant condition that necessitated the repair/replacement activity did not result from any examination, test or MANDE required by this Division. If the acceptance criterion for a particular item is not specified in this Division, the provisions of Division 1, IWA-3100(b) shall be employed for evaluation to determine the disposition.

(c) If no items met the criteria of (a) and (b) above, the term "None" should be recorded in the applicable table.

(d) If there are multiple reactors at a facility and inspection plans with different intervals, inspection periods, Editions, or Addenda, all shall be identified on each Form OAR-1.

(e) The respective Owner's Form OAR-1 shall be certified by the Owner and presented to the Inspector for the required signature.

RIM-6.2.3 Contracted Repair/Replacement Organization Responsibilities

Refer to Division 1, IWA-6212.

RIM-6.2.4 Owners' Repair/Replacement Certification Record NIS-2 Responsibilities

Refer to Division 1, IWA-6220.

RIM-6.3 RETENTION

RIM-6.3.1 Maintenance of Records

In addition to the provisions of Division 1, IWA-6310, the Owner shall retain records and reports identified in [RIM-6.3.3](#), [RIM-6.3.4](#), and [RIM-6.3.5](#).

RIM-6.3.2 Reproduction, Digitization, and Microfilming

Refer to Division 1, IWA-6320.

RIM-6.3.3 Construction Records

Refer to Division 1, IWA-6330.

RIM-6.3.4 RIM Program Records

The Owner shall designate the records to be maintained. Such records shall include the following, as applicable:

- (a) record index
- (b) the original RIM Program basis documents used for [RIM-1.1\(b\)](#)
- (c) RIM inspection plans, schedules and reports
- (d) records of flaw acceptance by analytical evaluation
- (e) records of regions in ferritic components with modified acceptance standards
- (f) nondestructive examination procedures

- (g) nondestructive examination records
- (h) MANDE personnel qualifications
- (i) leakage test procedures
- (j) leakage test records
- (k) monitoring procedures
- (l) monitoring records
- (m) records required by [Mandatory Appendix IV, Article IV-5](#)

RIM-6.3.5 Repair/Replacement Activity Records

The following records prepared in performance of a repair/replacement activity shall be retained:

- (a) evaluations required by Division 1, IWA-4160(a), IWA-4160(b), and IWA-4311
- (b) repair/replacement program and plans
- (c) records and reports of repair/replacement activities
- (d) reconciliation documentation
- (e) NIS-2 Forms
- (f) OAR-1 Forms
- (g) documents certifying repair/replacement activities by contracted Repair/Replacement Organizations

ARTICLE RIM-7

GLOSSARY

(21) RIM-7.1 TERMS AND DEFINITIONS

Specific terms used in this Division are found in Division 1, IWA-9000 and augmented in [Article RIM 7](#).

accident sequence: a representation in terms of an initiating event followed by a sequence of failures or successes of events (i.e., system, function, or operator performance) that can lead to undesired consequences, with a specified end state.

alternate requirements: monitoring or augmented NDE methodologies used to assess and evaluate component degradation other than the prescribed NDE methods contained in [Mandatory Appendix V](#) and any augmented provisions contained in the applicable reactor design supplement of [Mandatory Appendix VII](#).

availability: the probability that a system or component is capable of supporting its function.

capability category: a measure of the ability of a PRA to support risk-informed applications based on conformance to requirements established for PRA scope, level of detail, plant-specificity, and realism. Two levels are defined in the ASME/ANS PRA Standards, Capability Category I and II.

component exposure population: the set of equipment included in the scope of the RIM Program for which a particular RIM strategy is applied to influence reliability.

component-level requirement (CLR): CLRs are the allowable degradation limits of an individual component from a safety point of view. CLRs are described in accordance with the plant safety evaluation, using quantities such as the break size postulated in an accident scenario. Exceeding a CLR could lead to an increase in the CDF or CFF/LERF that has been calculated in the safety evaluation of the plant.

compressor: a mechanically driven device that increases the pressure and reduces the volume of a gas.

condition monitoring: the process of systematic data collection and evaluation to identify and quantify usage factors or changes in performance or condition of a SSC, such that remedial action may be planned to maintain SSC Reliability Targets.

containment failure frequency (CFF): CFF is the sum of frequencies of various containment failure modes ranging from small leaks to a large and early break of the containment.

core damage frequency (CDF): the expected number of core damage events per unit of time that involve the uncover and heatup of the reactor core to the point at which prolonged oxidation and severe fuel damage are anticipated and involving enough of the core to cause a significant release.

degradation mechanism: a phenomenon or process that attacks (e.g., wears, erodes, corrodes, cracks) the material under consideration.

event tree: a logic diagram that begins with an initiating event or condition and progresses through a series of branches that represent expected system or operator performance that either succeeds or fails and arrives at either a successful or failed end state.

event tree top event: the conditions (i.e., system behavior or operability, human actions, or phenomenological events) that are considered at each branch point in an event tree.

failure: events involving conditions that would disable a component's ability to perform its intended safety function.

failure mechanism: any of the processes that results in failure modes, including chemical, electrical, mechanical, physical, thermal, and human error.

false call probability (FCP): the percentage resulting from dividing the number of false calls by the number of unflawed specimens or unflawed grading units examined.

human error (HE): any human action that exceeds some limit of acceptability, including inaction where required, excluding malevolent behavior.

indication of degradation (ID): a signal or response that degradation exists that could lead to the exceedance of a CLR.

initiating event: any event that perturbs the steady state operation of the plant, if operating, or the steady state operation of the decay heat removal systems during shutdown operations such that a transient is initiated in the plant that leads to the need for reactor subcriticality and decay heat removal.

large early release frequency: (LERF): the expected number of large early releases per unit of time involving the rapid, unmitigated release of airborne fission products from the containment to the environment occurring

before the effective implementation of off-site emergency response and protective actions such that there is a potential for early health effects.

level of rigor: the level of confidence to which a given examination system must be demonstrated, based upon factors such as user needs, degradation mechanisms, and required Reliability Targets.

MANDE Program: a strategy and process of using Monitoring and NDE (MANDE) to meet SSC Reliability Targets. The MANDE Program is a subset of the RIM Program.

may: indicates an action that is permitted but not required.

monitoring: the systematic process of observing, tracking, and recording activities or data for the purpose of evaluating plant SSC conditions.

monitoring and nondestructive examination (MANDE): a term used in this Division that includes the activities of monitoring, NDE, and use of surveillance specimens, as established by the Monitoring and NDE Expert Panel.

piping system: an assembly of piping segments, piping supports, and other components with a defined function.

probabilistic risk assessment (PRA): a quantitative assessment of the event sequences involving the release of radioactive material; an estimate of accident frequencies, consequences and uncertainties.

probability of detection (POD): the percentage resulting from dividing the number of detections by the number of flawed specimens or flawed grading units examined. POD indicates the probability that an examination system will detect a given flaw.

reliability: the probability that a system or component will perform its specified function under given conditions upon demand and for a prescribed mission time.

reliability and integrity management (RIM): Those aspects of the plant design process that are applied to provide an appropriate level of reliability of SSCs and a continuing assurance over the life of the plant that such reliability is maintained. These include design features important to reliability performance such as design margins, selection of materials, testing and monitoring, provisions for maintenance, repair and replacement, leak testing, and NDE.

reliability target: A performance goal established for the probability that an SSC will complete its specified function in order to achieve plant-level risk and reliability goals.

RIM Program: a comprehensive program to define, evaluate, and implement strategies to ensure that Reliability Targets for SSCs are defined, achieved, and maintained throughout the plant lifetime as administered under RIM-2.

screening: a process that eliminates items from further consideration based on their negligible contribution to the probability of an accident or its consequences.

screening criteria: the values and conditions used to determine whether an item is a negligible contributor to the probability of an accident sequence or its consequences.

sizing accuracy: The difference between the actual length, depth, flaw separation, and remaining ligaments and the values measured using a nondestructive sizing technique as determined during the performance demonstration process.

shall: an action that is mandatory; i.e., a provision that the user is obliged to satisfy in order to comply with the standard.

should: an action that is not mandatory.

SSC: structure, system, component.

surveillance samples: specimens of SSC representative materials for monitoring the material performance, relevant to meeting the RIM target reliabilities, of inservice SSCs subjected to environmental stressors. Surveillance samples are located in the same or higher levels of environmental stressors as the inservice SSCs. They are unique for each reactor design, SSC design, and degradation mechanisms of concern.

uncertainty (as used in PRA): a representation of the confidence in the state of knowledge about the parameter values and models used in constructing the PRA.

uncertainty (as used in MANDE): a quantification representing the variability associated with monitoring and nondestructive examination (MANDE) data that includes many technique and application specific parameters such as the minimum detection capability, sizing accuracy, resolution tolerance, repeatability, consistency, etc.

MANDATORY APPENDIX I

RIM DECISION FLOWCHARTS FOR USE WITH THE RIM PROGRAM

ARTICLE I-1 FLOWCHARTS

(21) **I-1.1 GENERAL**

Figures I-1.1-1 through I-1.1-6 begin on the following page. Throughout the figures, the following symbols are used:

- (a) Unshaded circles denote inputs to the RIM Program.
- (b) Shaded circles and ovals denote inputs to the MANDE Program.
- (c) Unshaded octagons denote outputs for redesign.

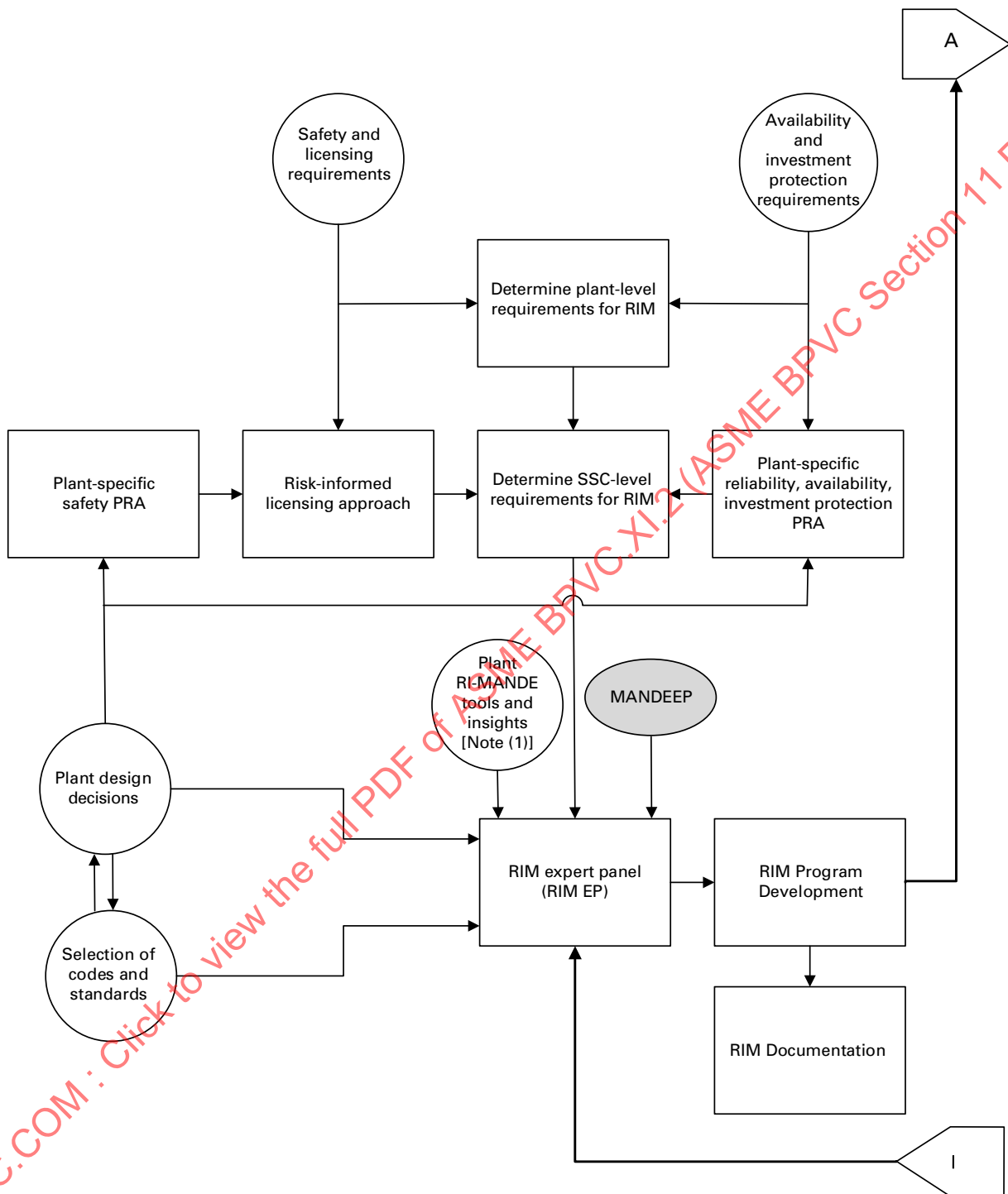
(d) Unshaded rectangles denote process elements.

(e) Shaded rectangles denote MANDE process elements.

(f) Diamonds denote decision points.

Thus, all symbols in the flow charts constitute the RIM Program and all shaded symbols in the flow charts constitute the MANDE Program.

(21)

Figure I-1.1-1 Inputs to the RIMEP for NPP Owner's RIM Program Development

NOTE: (1) The term "Plant RI-MANDE tools and insight" refers to the experience gained in deploying risk-informed (RI) ISI methodologies to the Section XI, Division 1 LWR fleet of reactors. This experience will grow as new reactor designs gain operating experience.

(21)

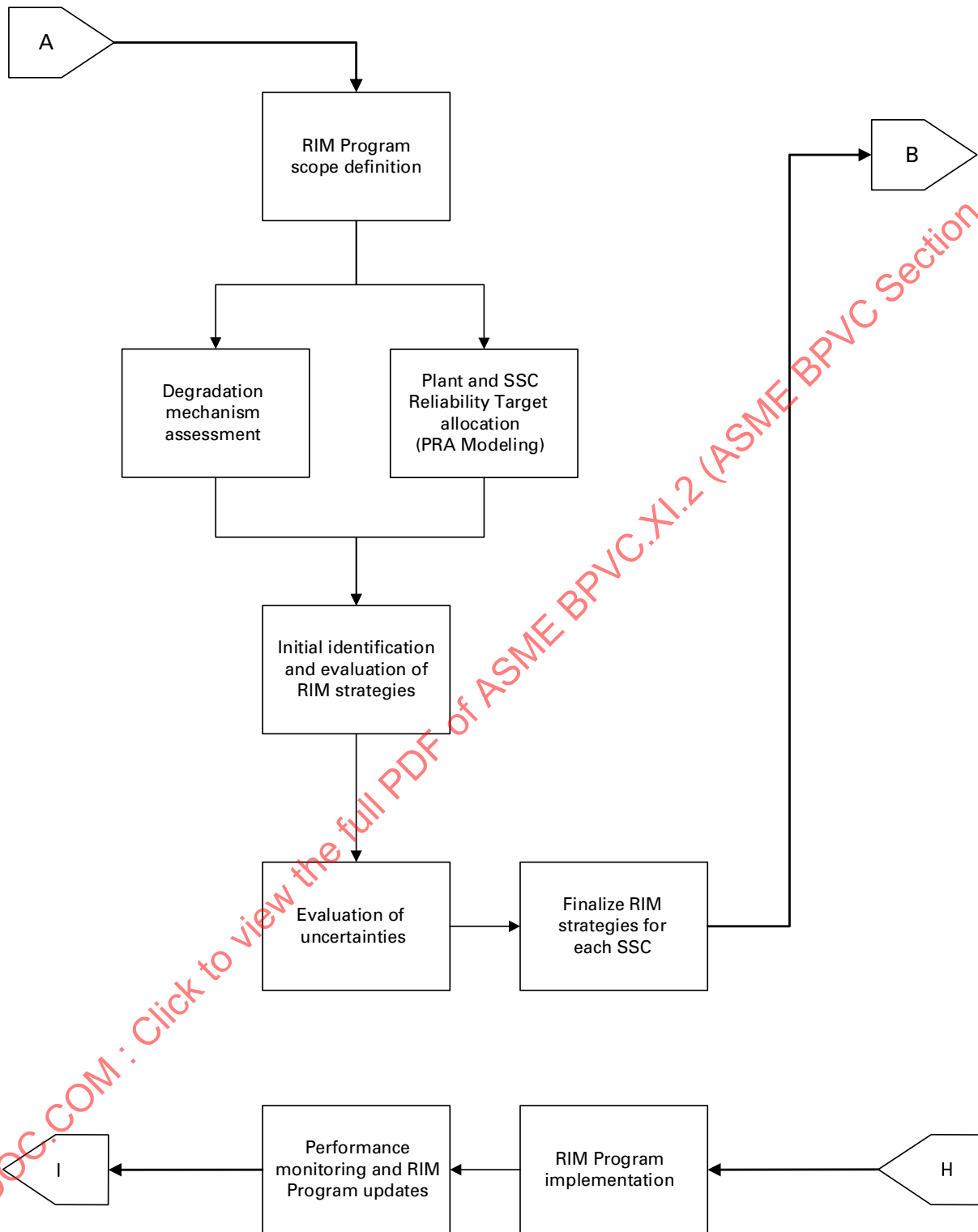
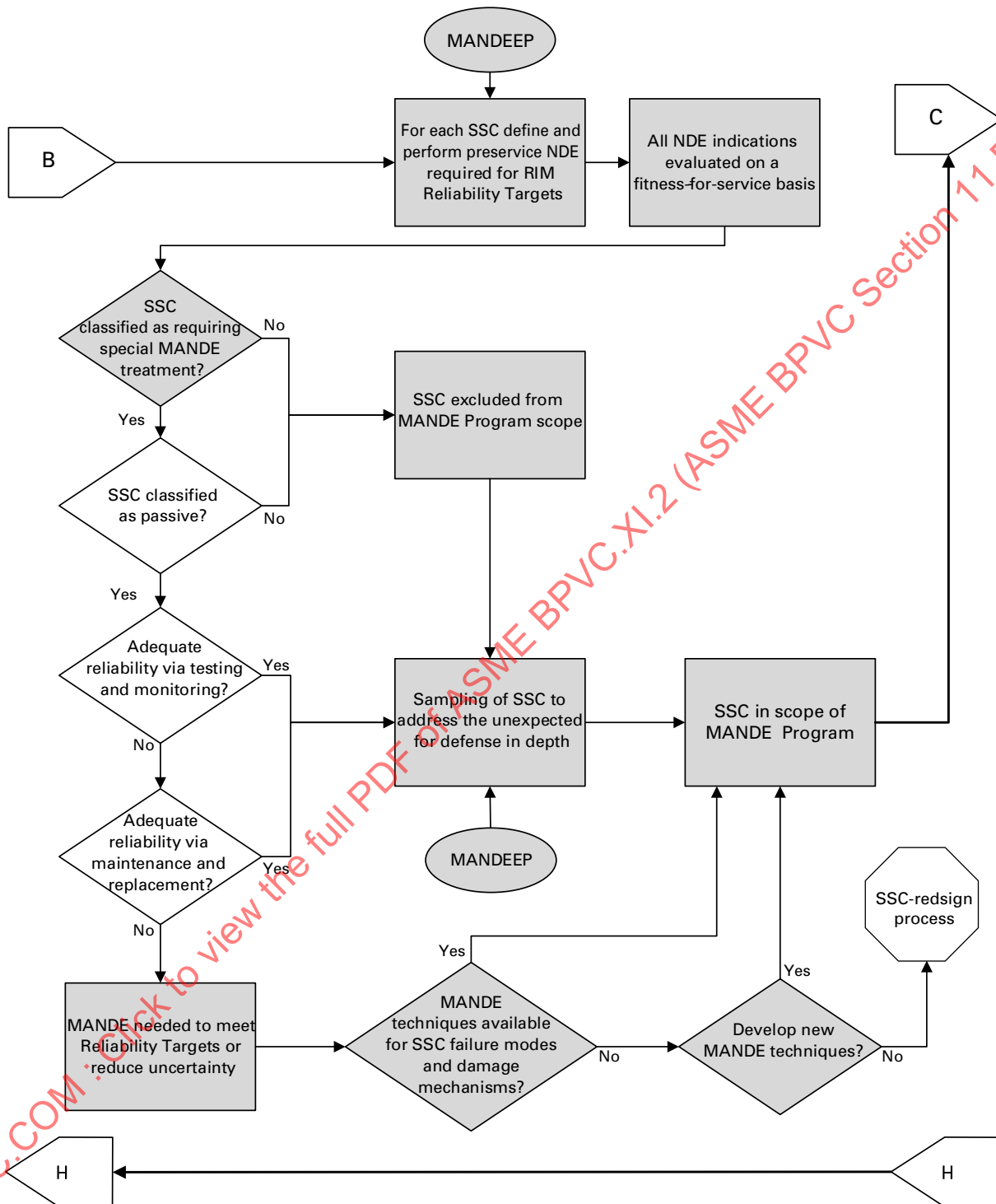
Figure I-1.1-2 RIM Program Development and Integration

Figure I-1.1-3 Process for Identifying the SSCs to Be in MANDE Program

(21)



(21)

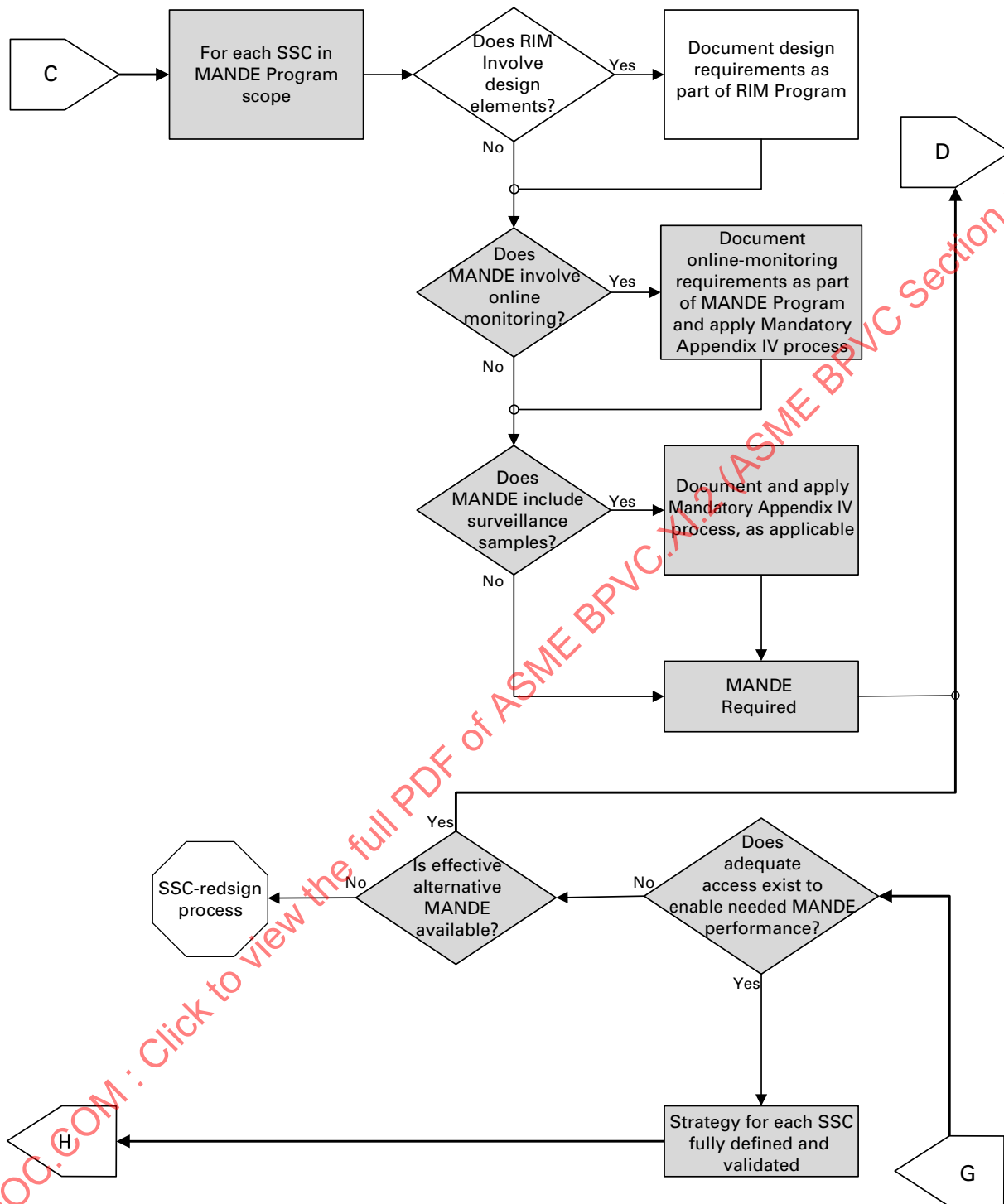
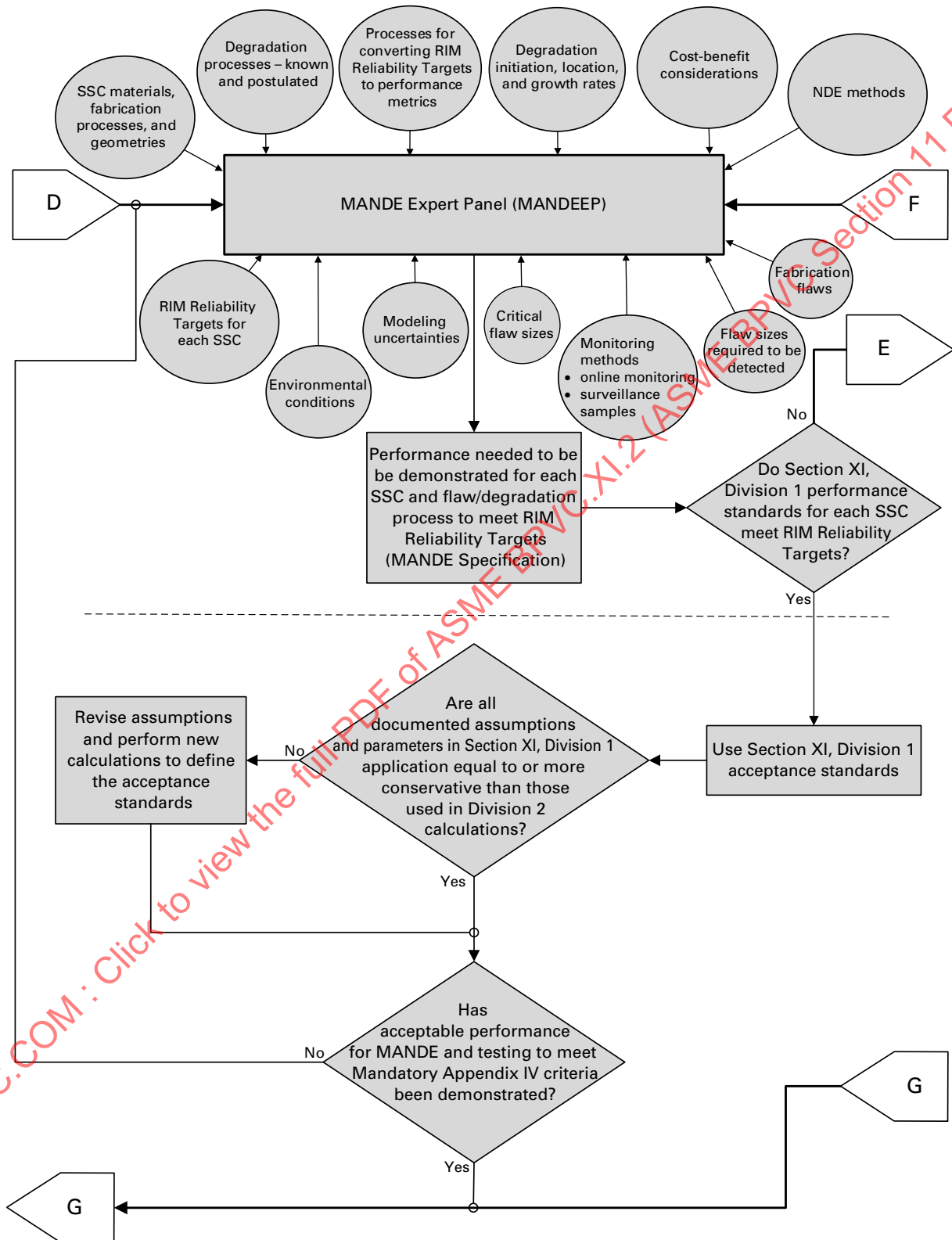
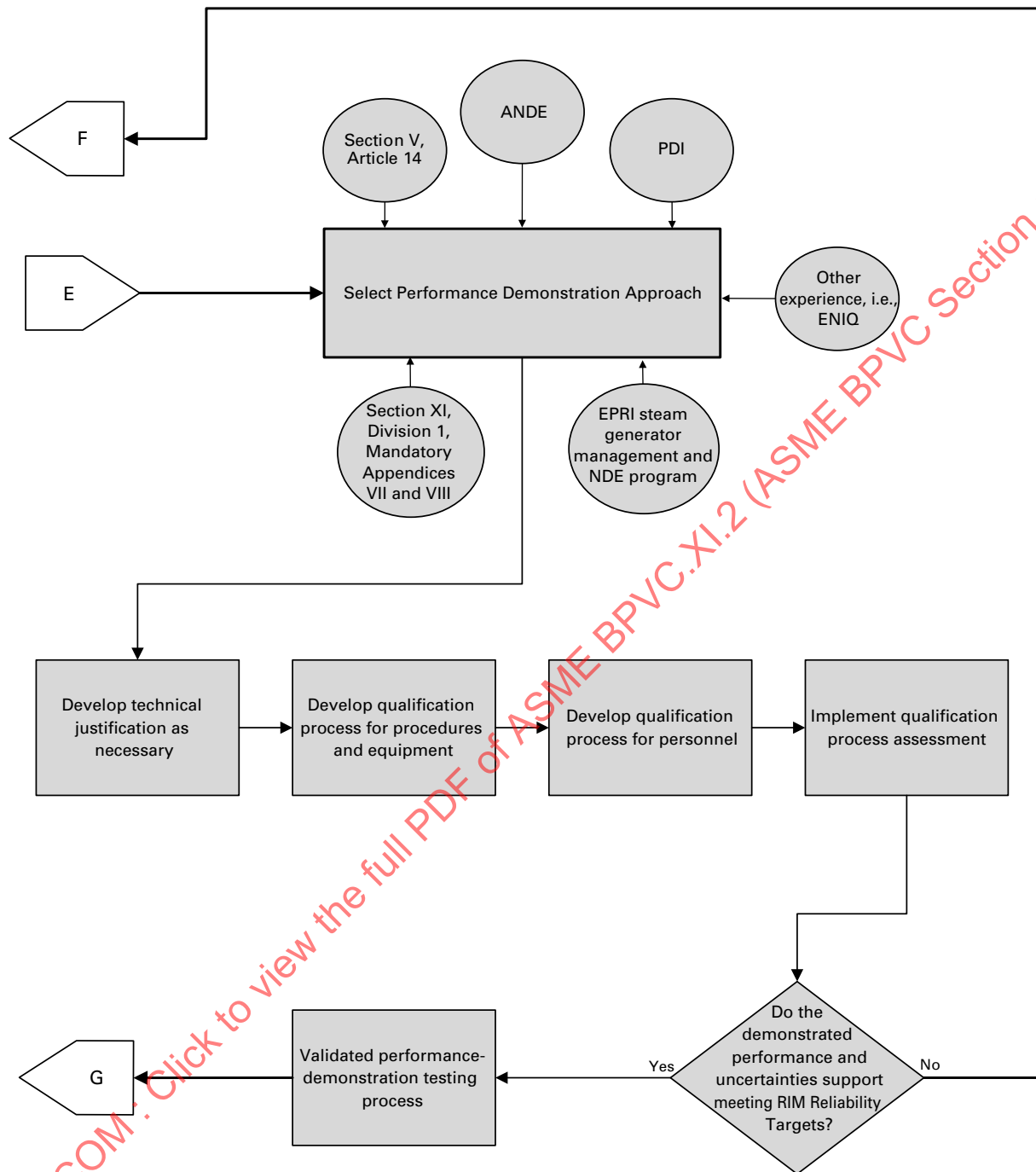
Figure I-1.1-4 Selection of Strategies for SSCs to Meet Reliability Targets

Figure I-1.1-5 Upper Half Shows Input to MANDEEP for Developing MANDE Specification and Lower Half Shows Process for Evaluating if Division 1 Requirements Meet MANDE Specifications (21)



(21) Figure I-1.1-6 Select, Develop, and Validate Performance Demonstration Approach to Meet SSC Reliability Target



Legend:

ANDE = ASME nondestructive examination
 ENIQ = European Network for Inspection and Qualification
 EPRI = Electric Power Research Institute
 PDI = Performance Demonstration Initiative

Figure I-1.1-7 Process for Evaluating Which SSCs to Include in RIM Program and Redesign Process

(21)

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MANDATORY APPENDIX II

DERIVATION OF COMPONENT RELIABILITY TARGETS FROM PLANT SAFETY REQUIREMENTS

ARTICLE II-1

GENERAL REQUIREMENTS

II-1.1 SCOPE

This Appendix shall be used for deriving component (or SSC) level requirements (CLRs) from plant-level safety requirements using probabilistic risk assessment (PRA). This Appendix provides a method for deriving CLRs in the form of SSC Reliability Targets.

II-1.2 ADEQUACY OF THE PRA

The PRA model as required by [RIM-2.4.3](#), shall be constructed so that it is applicable to derivation of component Reliability Targets from plant-level safety requirements.

II-1.3 PROCEDURE OVERVIEW

The derivation procedure includes the following steps:

- (a) Determine plant-level safety requirements in accordance with [II-2.1](#).
- (b) Allocate Reliability Targets in accordance with [II-2.2](#).
- (c) Identify groups of components in accordance with [II-2.3](#).
- (d) Assign candidate Reliability Targets to the groups in accordance with [II-2.4](#).
- (e) Evaluate impacts of the candidate Reliability Targets on plant level risks in accordance with [II-2.5](#).
- (f) Determine the combination of Reliability Target values for the components in accordance with [II-2.6](#).

ARTICLE II-2

RELIABILITY TARGET DERIVATION

II-2.1 PLANT-LEVEL SAFETY REQUIREMENTS

(a) For light water reactor (LWR) types use the plant-level safety goals that are established in terms of Core Damage Frequency (CDF) and Large Early Release Frequency (LERF).

(b) For advanced non-LWR types, such as the High-Temperature Gas Reactor (HTGR), use appropriate plant-level safety goals, based on metrics such as regulatory limits on the risks, frequencies, and radiological consequences of licensing basis events.

(c) If quantitative plant-level safety requirements are available, based on metrics such as CDF, Containment Failure Frequency (CFF) or LERF, SSC Reliability Targets as obtained herein may be used as CLRs.

II-2.2 ALLOCATION OF RELIABILITY TARGETS

(a) The objective of setting Reliability Targets for SSCs in the scope of the RIM Program is to establish a reference point against which to judge system performance to meet the plant level safety requirements. The reliability targets that the owner assigns to SSCs should be consistent with the plant level safety goals and should consider industry-wide operating experience where practicable.

(b) Reliability targets may be developed during the initial phase of the RIM Program. These targets are intended to be compared with actual plant performance to identify deviations from expected performance.

(c) The Reliability Target allocation includes the following considerations:

(1) Quantitative plant-level requirements may be divided and distributed for each PRA scope identified by the type of initiating events, initial plant operating states, and accident sequences.

(2) Accident categories shall be identified for each PRA scope based on the PRA model, and a Reliability Target. The Reliability Target allocated for the PRA scopes shall be divided and distributed for each accident category.

(3) The event trees relevant to passive component failures shall be identified for the accident category. The event tree top events (e.g., see ASME/ANS RA-S-1.4-2013) related to dynamic component failures and human errors may be removed by assuming that

their probability is 1. The sequences depending only on dynamic functions shall be excluded from the event trees. Reliability Targets allocated for the accident category shall be divided and distributed for the accident category due to passive component failures and other contributors.

(4) Information on design and operation, and past PRA studies, shall be used for allocation of Reliability Targets.

II-2.3 IDENTIFICATION OF COMPONENT GROUPS

Groups of components for which loss of function would have the same effect on the PRA model as identified in II-2.2(c)(3) shall be identified.

II-2.4 TRIAL ASSIGNMENT OF RELIABILITY TARGETS

(a) Candidate Reliability Targets for the frequency or probability of structural integrity loss shall be assigned to the groups identified in II-2.3.

(b) Information on design and operation and past PRA studies shall be used for identification of candidate Reliability Targets.

II-2.5 EVALUATION OF IMPACTS OF RELIABILITY TARGETS ON PLANT-LEVEL RISK

(a) Risk indices given as quantitative plant-level requirements (e.g., CDF) shall be evaluated using the PRA model identified in II-2.2(c)(3) using the candidate Reliability Target of the groups identified in II-2.3.

(b) The combinations of candidate Reliability Targets necessary and sufficient to achieve the allocated Reliability Target for the accident categories due to passive component failures in II-2.2(c)(3) shall be selected.

II-2.6 DETERMINATION OF RELIABILITY TARGETS

A suitable combination of Reliability Targets shall be chosen from the candidates selected in II-2.5 by considering the balance of Reliability Targets among the groups identified in II-2.3.

MANDATORY APPENDIX III OWNER'S RECORD AND REPORT FOR RIM PROGRAM ACTIVITIES

ARTICLE III-1 GUIDES TO COMPLETING FORMS

III-1.1 FORM OAR-1

See Division 1, Mandatory Appendix II for Form OAR-1.
See [Table III-1.1-1](#) for instructions on completing Form OAR-1.

III-1.2 FORM NIS-2

See Division 1, Mandatory Appendix II for Form NIS-2 and the instructions for completing it.

Table III-1.1-1 Guide for Completing Form OAR-1

(21)

Reference to Circled Numbers in Form OAR-1	Description
1	A unique number to identify the report.
2	The name and address of the nuclear plant where the inservice examinations, MANDE, and tests were performed. If multiple reactors are located at a single plant, each reactor shall be uniquely identified.
3	The Owner's designated unit identification number.
4	The date determined by the Owner that the unit originally became available for regular production of electricity or process heat.
5	The unique number assigned to the refueling/maintenance outage.
6	Successive RIM interval and duration of the RIM interval.
7	Inspection period within the RIM interval (first, second, or third).
8	The Edition of Section XI applicable to the MANDE and tests represented by the Form.
9	The date and revision level of the inspection plan followed during the MANDE and tests represented by this Form.
10	The Edition of Section XI applicable to the MANDE and tests represented if different from that in number 8 above.
11	Applicable Construction Code or Section XI Code Cases associated with the repair/replacement activity.
12	Same number as in number 5 above.
13	Signature and title of the Owner's Designee who certifies the accuracy of the report.
14	The date this Form was prepared.
15	The name of the Inspector's employer, the Authorized Inspection Agency.
16	The address of the Authorized Inspection Agency (city/town and state or province).
17	Authorized Nuclear Inservice Inspector's signature.
18	Authorized Nuclear Inservice Inspector's National Board Commission Number, including endorsements and, if applicable, justification name and Certificate of the competency number held in the state or province where inspections represented by this Form OAR-1 were performed.
19	The date (month, day, year) the Authorized Nuclear Inservice Inspector signed the Form.
20	Examination category from Mandatory Appendix V , or MANDE alternatives established by Nonmandatory Appendix A .
21	Brief description of indication or "None."
22	Resolution of indication.
23	Construction Code safety classification used for construction.
24	Item description.
25	Indicate "Repair" or "Replacement."
26	Date repair/replacement plan completed.
27	Unique repair/replacement plan number.
28	Describe any additional information not otherwise covered in Owner's Activity Report.

MANDATORY APPENDIX IV MONITORING AND NDE QUALIFICATION

ARTICLE IV-1 INTRODUCTION

(21) IV-1.1 SCOPE

This Appendix provides requirements for performance-based qualification of monitoring and nondestructive examination (MANDE) methods and techniques. It addresses qualification of the personnel, procedures, and equipment. The qualification requirements described herein support the Reliability Targets identified in the Owner's Design Specification based on RIM Reliability Targets for examination of the applicable structure, system, or component (SSC) as required by [RIM-2.7.6](#). This process is described in [Mandatory Appendix I, Figures I-1.1-1 through I-1.1-6](#) and the following paragraphs.

IV-1.2 METHODS

The following NDE and monitoring methods are addressed in this Appendix:

- (a) acoustic emission (AE)
 - (1) leak detection
 - (2) defect and degradation and damage detection
- (b) eddy current (ET)
- (c) leak testing (LT)
 - (1) helium mass spectrometer testing
 - (2) halogen diode leak testing
 - (3) ultrasonic leak detection
 - (4) pressure change testing
 - (5) bubble testing
- (d) liquid penetrant (PT)
- (e) magnetic particle (MT)
- (f) online monitoring (e.g., leak detection, vibration analysis, thermal sensors) and additional monitoring methods as determined by the Monitoring and NDE Expert Panel (MANDEEP)
- (g) radiographic examination (RT)
- (h) ultrasonic examination (UT)
- (i) visual examination (VT) (VT-1, VT-2, or VT-3)
- (j) surveillance samples

IV-1.3 OWNER'S REQUIREMENTS

IV-1.3.1 General Requirements

The MANDEEP is responsible for the following, consistent with the Reliability Targets established by RIMEP, or as identified in the Design Specification prepared by the Owner, for the applicable SSCs:

- (a) fulfilling the requirements of [IV-1.3.2](#)
- (b) planning of examinations
- (c) maintenance of calibration standards
- (d) records and record retention

IV-1.3.2 Owner's Monitoring and NDE Expert Panel (MANDEEP)

IV-1.3.2.1 Responsibilities. The MANDEEP shall be (21) responsible for establishing and documenting the following:

- (a) the MANDE specification ([Figure I-1.1-5](#)).
 - (b) the level of rigor required for MANDE qualification. For NDE, reference requirements are as defined for Section V, Article 14.
 - (c) specific examination requirements, including coverage, frequency, location, and volume.
 - (d) a minimum criteria of MANDE for all SSCs. This shall be based upon the following:
 - (1) the Reliability Target value established for individual SSCs
 - (2) degradation mechanisms and stressors assigned to the SSC
 - (3) the detection capability and associated uncertainty of the MANDE methods proposed for each application
 - (4) relevant design and operating factors specific to a given reactor type
- This applies to all SSCs in the RIM Program and sampling of other SSCs that may have been exempted but which are deemed essential for defense-in-depth. All of the knowns, assumptions, decisions, and the technical basis for the process chosen shall be documented in the MANDE Specification.

(e) acceptance criteria for evaluation of monitoring or NDE indications identified.

IV-1.3.2.2 MANDEEP Qualifications. The following requirements shall apply to the Monitoring and NDE Expert Panel (MANDEEP):

(a) The MANDEEP shall identify and oversee development of MANDE methods for examinations of identified items, by specifying a validation strategy and process designed to demonstrate achieving the required performance that supports achieving the RIM Reliability Target. The MANDEEP shall specify criteria for qualification of methods, techniques and procedures. The MANDEEP shall also specify criteria for qualification and certification of examination personnel. The MANDEEP's work shall be independent from production and operational concerns, shall be provided with full access to necessary data, and shall additionally be adequately resourced to be able to complete its work. MANDEEP members may be either part of the Owners' organization or independently contracted.

(b) The panel shall be formed by and shall be responsible to the Panel Chair. The Chair shall have a broad-based knowledge of nondestructive examination, engineering mechanics, materials, welding and joining, statistics, and radiation safety in order to select expert panel members. The Chair shall hold a 4-yr technical degree from an accredited college or university. In addition, the Chair shall have 15 yr of related experience in NDE (e.g., examination, research, teaching), including 10 yr of experience in the application of monitoring and NDE at nuclear power plants. The Chair shall have functional independence within the plant Owner's organization, similar to independence that is afforded to Quality Assurance functions. The MANDEEP Chair shall be a member of the RIMEP.

(c) The MANDEEP's initial make up shall be determined by the Chair and shall include members with in-depth knowledge of surface and volumetric NDE methods and techniques and the following:

- (1) failure modes both known and postulated
- (2) engineering mechanics, materials, and fabrication processes

(3) degradation initiation, location, and growth rates
(4) critical flaw sizes and flaw sizes required to be detected during performance demonstration

(5) fabrication flaws requiring detection and accurate characterization

(6) monitoring methods including online techniques

(7) cost-benefit considerations

(8) converting RIM Reliability Targets into MANDE performance metrics

(9) testing methodology for performance demonstrations and

(10) operational knowledge of specific nuclear power plant design

(d) MANDEEP members shall be selected based on their expertise in a given subject or discipline that contributes to the assigned effort. MANDEEP membership is not based on a detailed education or experience criteria. It shall be based on the individual's expertise in the subject matter and this expertise shall be documented to justify their selection. Where methods or techniques are detailed in a Code or standard and a recognized certification is applicable at least one MANDEEP member shall be certified equivalent to NDE Level III. For methods or techniques, which are not standardized, or in development, at least one MANDEEP member shall be a senior representative of the developing organization.

(e) The Chair shall establish the panel with membership initially based on informed assumptions as to the technologies and confidence necessary to achieve the RIM Reliability Targets for each SSC within the RIM Program. The Chair shall prepare a document addressing the basis for panel formation. The basis document shall outline potential monitoring and NDE (MANDE) methods or techniques and prioritize their potential to meet examination objectives. This basis document shall be reviewed and validated or modified as determined by the panel formed. The basis document shall describe staffing of the MANDEEP, the work schedule, and funding necessary to conduct the activities defined in this basis document.

ARTICLE IV-2

PROCEDURES, EQUIPMENT, AND PERSONNEL REQUIREMENTS

(21) **IV-2.1 BASIC QUALIFICATION (FIGURES I-1.1-1 THROUGH I-1.1-6)**

The MANDEEP shall establish programmatic procedures to control personnel qualification in accordance with the following:

(a) the ASME Nondestructive Examination and Quality Control Central Qualification and Certification Program (ANDE-1) Standard, or

(b) the national or international central certification program required by the regulatory and enforcement authorities having jurisdiction at the plant site,

(c) for methods or techniques not addressed by (a) or (b), the Owner's program for NDE personnel qualification shall apply,

(d) where personnel qualification programs for MANDE methods exist, the MANDEEP shall review for acceptance. Where qualification programs do not exist or are not acceptable, the MANDEEP shall specify qualification requirements. These qualification requirements shall be based on performance-based qualification principles similar to those included in the ANDE-1 Standard.

IV-2.2 METHOD/TECHNIQUE PERSONNEL SPECIFIC QUALIFICATIONS

IV-2.2.1 Data Acquisition Personnel

Personnel performing only data acquisition shall have received specific training and shall be qualified in accordance with the Owner's procedures for the applicable equipment operation and data recording tasks. These qualification requirements shall be based on performance-based qualification principles similar to those included in ASME ANDE-1.

IV-2.2.2 Data Evaluation Personnel

Personnel performing evaluation of examination data shall have received specific training in the data evaluation techniques used in performance demonstration and shall successfully complete the performance demonstration required in Article IV-4.

ARTICLE IV-3

RELIABILITY-BASED QUALIFICATION OF MONITORING AND NDE (MANDE) METHODS AND TECHNIQUES

IV-3.1 GENERAL

The MANDEEP shall be responsible for determining the performance demonstration requirements for each SSC to reach the Reliability Target based on applicable flaw damage mechanisms, degradation processes, and frequency of examination.

IV-3.2 DETERMINATION OF THE QUALIFICATION REQUIREMENTS

To establish the requirements for qualification of a MANDE method and technique for an SSC, the MANDEEP shall consider factors relevant to maintaining the Reliability Target including the following:

- (a) materials and fabrication processes
- (b) part geometry
- (c) stress analysis, including the effect of known or postulated fabrication flaws
- (d) known and postulated degradation mechanisms
- (e) flaw/condition initiation and growth rates
- (f) critical flaw size or condition extent (e.g., material loss)
- (g) minimum flaw size or condition extent required for detection
- (h) sizing accuracy (i.e., length, depth, flaw separation, remaining ligament, etc.)
- (i) flaw location and coverage of examination
- (j) sample size and distribution
- (k) frequency of examination
- (l) probability of detection and false calls
- (m) accuracy of the MANDE technique

IV-3.3 QUALIFICATION PROCESS

IV-3.3.1 General

The qualification of a MANDE method supports the Reliability Target for the SSC determined as a result of consideration of the factors listed in IV-3.2. The achieved reliability of the MANDE method shall be then considered by the MANDEEP in determining any additional controls needed to achieve the necessary Reliability Target of the SSC.

IV-3.3.2 SSC MANDE Specifications (Figure I-1.1-5) (21)

A MANDE Specification is required for the qualification of monitoring and NDE for each SSC. The MANDE Specification is a document describing the MANDE methods, techniques, and required performance to be used for a specific SSC. It shall include a reference to the supporting Technical Justification, which shall include the principles of the technique as applied to the SSC, an explanation of the procedure, including the equipment to be used, and any relevant laboratory and field experience.

IV-3.3.3 MANDE Technical Justification (Figure I-1.1-6)

For each method and technique identified in the MANDE Specification, a Technical Justification shall be prepared. For NDE, reference requirements are as defined for Section V, Article 14. In addition, the Technical Justifications shall specifically address the application of the method and technique to each SSC for which it is identified in the MANDE Specification.

IV-3.3.4 Levels of Rigor (Figure I-1.1-6)

(a) The MANDEEP is responsible for establishing the levels of rigor required for qualification for each SSC based on the Reliability Target required. For NDE, reference requirements are as defined for Section V, Article 14.

(b) A High Level of Rigor is generally required to support a probabilistic risk assessment (PRA) and includes a sufficient number of test specimens to effectively quantify uncertainties, estimate sizing error distributions, and determine a Probability of Detection (POD) for specific degradation mechanisms or flaw types, locations, and sizes.

IV-3.3.5 Qualification of NDE Methods and Techniques (Figure I-1.1-6)

The qualification process for each NDE Method and Technique shall be defined in a written procedure approved by the MANDEEP. The written procedure shall include the test specimen requirements and essential variable ranges bounding the qualification. Essential variables shall include but are not limited to hardware, equipment settings, operational input values, and software

revisions that directly affect the calibration, data acquisition, and analysis parameters. Changes in essential variables of a demonstrated procedure shall not be allowed without requalification of the procedure.

IV-3.3.6 Monitoring Methods and Techniques **(Figure I-1.1-6)**

Special requirements for qualification of monitoring methods and techniques shall be established and defined in a written procedure approved by the MANDEEP. The written procedure shall address the requirements and essential variable ranges bounding the qualification demonstration. Changes in essential vari-

ables of a demonstrated procedure shall not be allowed without requalification of the procedure.

IV-3.3.7 Qualification Alternatives

Alternative qualifications for MANDE methods and techniques that have been previously established by existing industry programs accepted by the regulatory and enforcement authorities having jurisdiction at the plant site may be used for methods and techniques to the extent that the MANDEEP determines that they are sufficient to support Reliability Target requirements for the applicable SSCs.

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ARTICLE IV-4

PERFORMANCE DEMONSTRATIONS FOR MANDEE PERSONNEL

(FIGURE I-1.1-6)

IV-4.1 GENERAL

Qualification of personnel shall be performed as a blind test where the candidate has no knowledge of the contents of the specimen test set. The specimen test set may include flaws or degradation mechanisms used for the method and technique procedure qualification (see [Article IV-3](#)) or from other specimens fabricated specifically for the personnel qualification as determined by the MANDEEP.

IV-4.2 PERFORMANCE DEMONSTRATION FOR PERSONNEL FOR MONITORING METHODS

Performance Demonstration requirements for personnel for monitoring methods and techniques, commensurate with their roles and responsibilities, shall be

established and defined in a written procedure approved by the MANDEEP.

IV-4.3 PERFORMANCE DEMONSTRATION FOR NDE PERSONNEL

NDE Personnel Performance Demonstrations shall be conducted in accordance with a written procedure approved by the MANDEEP that includes the number of test specimens; the number, location, and size or extent of flaws or degradation mechanisms; and the pass/fail criteria established as necessary to support the Reliability Target of each SSC in conjunction with the qualification for the applicable NDE method and technique.

ARTICLE IV-5 RECORDS

IV-5.1 GENERAL

Records shall be prepared and maintained as required in [Article RIM-6](#). Additionally, records shall be maintained in support of the qualification program and shall include the MANDE Specifications, Technical Justifications, and written procedures. Additional records shall be maintained for performance demonstrations for each MANDE method and technique as well as for personnel performance demonstrations. Record retention requirements shall be established by the MANDEEP.

IV-5.2 RECORDS FOR METHODS AND TECHNIQUE QUALIFICATION

The following shall be prepared, reviewed, and maintained:

- (a) the SSC MANDE Specifications (see [IV-3.3.2](#))
- (b) the Technical Justification (see [IV-3.3.3](#))
- (c) the written procedures for qualification process for each method and technique (see [IV-3.3.5](#) and [IV-3.3.6](#))

IV-5.3 RECORDS FOR PERSONNEL PERFORMANCE DEMONSTRATIONS

The written procedures in accordance with [IV-4.2](#) and [IV-4.3](#) shall be maintained.

MANDATORY APPENDIX V

CATALOG OF NDE REQUIREMENTS AND AREAS OF INTEREST

ARTICLE V-1 TABLES

V-1.1 GENERAL

(a) If multiple SSCs of similar configuration (e.g., steam generators, attachments to SSCs) exist at a single facility, MANDEEP shall determine the extent of MANDE that shall be applied to each individual SSC or attachment in consideration of the applicable degradation mechanisms that apply and the required reliability target value that the SSC must satisfy.

(b) The Tables in this Appendix make reference to Division 1 examination categories and examination volumes. These references are not intended to imply that either Class 1 or Class 2 Division 1 requirements are to be used for a particular RIM SSC. Once an SSC is selected

for incorporation into the RIM Program, it no longer carries a class designation that may have been used for construction of the SSC. The referenced Division 1 figures in this Appendix are solely to denote typical geometries for various SSC containing welds and related examination volumes that should be considered by the MANDEEP, provided that such welds are specifically included in RIM SSC MANDE population. RIM MANDE is not limited to weld centric examination requirements. Base material MANDE may be equal to or more critical for maintaining the Reliability Target of an SSC, based on assigned degradation mechanisms, than merely weld volume examinations (e.g., creep).

Table V-1.1-1 Examination Category A, Pressure-Retaining Welds in Reactor Vessels

Item No.	Parts Examined	Examination Requirements/ Figure No.	Examination Method	Acceptance Standard
1.10	Shell welds			
1.11	Circumferential	IWB-2500-1	Volumetric	Article RIM-3 (VII-1.4.1, VII-3.4.1)
1.12	Longitudinal (all welds)	IWB-2500-2	Volumetric	Article RIM-3 (VII-1.4.1, VII-3.4.1)
1.20	Head welds			
1.21	Circumferential	IWB-2500-3	Volumetric	Article RIM-3 (VII-1.4.1, VII-3.4.1)
1.22	Meridional (all welds)	IWB-2500-3	Volumetric	Article RIM-3 (VII-1.4.1, VII-3.4.1)
1.30	Shell-to-flange	IWB-2500-4	Volumetric	Article RIM-3 (VII-1.4.1, VII-3.4.1)
1.40	Head-to-flange	IWB-2500-5	Volumetric and surface [Note (1)]	Article RIM-3 (VII-1.4.1, VII-3.4.1)
1.50	Repair areas [Note (2)]	IWB-2500-1 and IWB-2500-2	Volumetric	Article RIM-3 (VII-1.4.1, VII-3.4.1)
1.51	Beltline region	IWB-2500-1 and IWB-2500-2	Volumetric	Article RIM-3 (VII-1.4.1, VII-3.4.1)

NOTES:

- (1) After a preservice or inservice ultrasonic examination has been performed with no flaw detected that exceeds the acceptance criteria of VII-1.4.1 or VII-3.4.1, only the surface examination requirements of 1.40 need to be met.
- (2) Material (base material) weld repairs where repair depth exceeds 10% nominal of the vessel wall. If the location of the repair is not positively and accurately known, then the individual shell plate, forging, or shell course containing the repair shall be included.

Table V-1.1-2 Examination Category B, Pressure-Retaining Welds in Vessels Other Than Reactor Vessels

Item No.	Parts Examined	Examination Requirements/ Figure No.	Examination Method	Acceptance Standard
Pressurizer				
2.10	Shell-to-head			
2.11	Circumferential	IWB-2500-1	Volumetric	Article RIM-3 (VII-1.4.1, VII-3.4.1)
2.12	Longitudinal	IWB-2500-2	Volumetric	Article RIM-3 (VII-1.4.1, VII-3.4.1)
2.20	Head welds			
2.21	Circumferential	IWB-2500-3	Volumetric	Article RIM-3 (VII-1.4.1, VII-3.4.1)
2.22	Meridional	IWB-2500-3	Volumetric	Article RIM-3 (VII-1.4.1, VII-3.4.1)
Steam Generators (Primary Side)				
2.30	Head welds			
2.31	Circumferential	IWB-2500-3	Volumetric	Article RIM-3 (VII-1.4.1, VII-3.4.1)
2.32	Meridional	IWB-2500-3	Volumetric	Article RIM-3 (VII-1.4.1, VII-3.4.1)
2.40	Tubesheet-to-head welds	IWB-2500-6	Volumetric	Article RIM-3 (VII-1.4.1, VII-3.4.1)
Heat Exchangers (Primary Side) — Head				
2.50	Head welds			
2.51	Circumferential	IWB-2500-1, IWB-2500-3	Volumetric	Article RIM-3 (VII-1.4.1, VII-3.4.1)
2.52	Meridional	IWB-2500-3	Volumetric	Article RIM-3 (VII-1.4.1, VII-3.4.1)
Heat Exchangers (Primary Side) — Shell				
2.60	Tubesheet-to-head welds	IWB-2500-6	Volumetric	Article RIM-3 (VII-1.4.1, VII-3.4.1)
2.70	Longitudinal welds (all welds)	IWB-2500-2	Volumetric	Article RIM-3 (VII-1.4.1, VII-3.4.1)
2.80	Tubesheet-to-shell welds	IWB-2500-6	Volumetric	Article RIM-3 (VII-1.4.1, VII-3.4.1)
2.90	Tubes to tubesheet	TBD	Volumetric	TBD
2.100	Tubes	TBD	Volumetric	TBD

Table V-1.1-3 Examination Category D, Full-Penetration Welded Nozzles in Vessels

Item No.	Parts Examined	Examination Requirements/ Figure No.	Examination Method	Acceptance Standard
Reactor Vessel				
3.90	Nozzle-to-vessel welds	IWB-2500-7 [Note (1)]	Volumetric	Article RIM-3 (VII-1.4.2, VII-3.4.2)
3.100	Nozzle inside radius section	IWB-2500-7 [Note (1)]	Volumetric	Article RIM-3 (VII-1.4.2, VII-3.4.2)
Pressurizer				
3.110	Nozzle-to-vessel welds	IWB-2500-7 [Note (1)]	Volumetric	Article RIM-3 (VII-1.4.2, VII-3.4.2)
Steam Generators (Primary Side)				
3.130	Nozzle-to-vessel welds	IWB-2500-7 [Note (1)]	Volumetric	Article RIM-3 (VII-1.4.2, VII-3.4.2)
Heat Exchanger				
3.150	Nozzle-to-vessel welds	IWB-2500-7 [Note (1)]	Volumetric	Article RIM-3 (VII-1.4.2, VII-3.4.2)
3.160	Nozzle inside radius section	IWB-2500-7 [Note (1)]	Volumetric	Article RIM-3 (VII-1.4.2, VII-3.4.2)
3.170	Nozzle-to-nozzle welds	IWB-2500-7 [Note (1)]	Volumetric	Article RIM-3 (VII-1.4.2, VII-3.4.2)

NOTE: (1) The examination volumes shall apply to the applicable figure shown in Division 1, Figures IWB-2500-7(a) through IWB-2500-7(d).

Table V-1.1-4 Examination Category F, Pressure-Retaining Dissimilar Welds in Vessel Nozzles

Item No.	Parts Examined	Examination Requirements/ Figure No.	Examination Method	Acceptance Standard
Reactor Vessel				
5.10	NPS 4 (DN 100) or larger nozzle to safe end butt welds	IWB-2500-8	Volumetric and surface	Article RIM-3 (VII-1.4.3, VII-3.4.3)
5.11	NPS 4 (DN 100) or larger nozzle to component butt welds	IWB-2500-8	Volumetric and surface	Article RIM-3 (VII-1.4.3, VII-3.4.3)
5.20	Less than NPS 4 (DN 100) nozzle to safe end butt welds	IWB-2500-8	Volumetric or surface	Article RIM-3 (VII-1.4.3, VII-3.4.3)
5.30	Nozzle to safe end socket welds	IWB-2500-8	Volumetric or surface	Article RIM-3 (VII-1.4.3, VII-3.4.3)
Pressurizer				
5.40	NPS 4 (DN 100) or larger nozzle to safe end butt welds	IWB-2500-8	Volumetric and surface	Article RIM-3 (VII-1.4.3, VII-3.4.3)
5.50	Less than NPS 4 (DN 100) nozzle to safe end butt welds	IWB-2500-8	Volumetric or surface	Article RIM-3 (VII-1.4.3, VII-3.4.3)
5.60	Nozzle to safe end socket welds	IWB-2500-8	Volumetric or surface	Article RIM-3 (VII-1.4.3, VII-3.4.3)
Steam Generator				
5.70	NPS 4 (DN 100) or larger nozzle to safe end butt welds	IWB-2500-8	Volumetric and surface	Article RIM-3 (VII-1.4.3, VII-3.4.3)
5.71	NPS 4 (DN 100) or larger nozzle to component butt welds	IWB-2500-8	Volumetric and surface	Article RIM-3 (VII-1.4.3, VII-3.4.3)
5.80	Less than NPS 4 (DN 100) nozzle to safe end butt welds	IWB-2500-8	Volumetric or surface	Article RIM-3 (VII-1.4.3, VII-3.4.3)
5.90	Nozzle to safe end socket welds	IWB-2500-8	Volumetric or surface	Article RIM-3 (VII-1.4.3, VII-3.4.3)
Heat Exchanger				
5.100	NPS 4 (DN 100) or larger nozzle to safe end butt welds	IWB-2500-8	Volumetric and surface	Article RIM-3 (VII-1.4.3, VII-3.4.3)
5.110	Less than NPS 4 (DN 100) nozzle to safe end butt welds	IWB-2500-8	Volumetric or surface	Article RIM-3 (VII-1.4.3, VII-3.4.3)
5.120	Nozzle to safe end socket welds	IWB-2500-8	Volumetric or surface	Article RIM-3 (VII-1.4.3, VII-3.4.3)

Table V-1.1-5 Examination Category G-1, Pressure-Retaining Bolting Greater Than 2 in. (50 mm) in Diameter

Item No.	Parts Examined	Examination Requirements/ Figure No.	Examination Method	Acceptance Standard
Reactor Vessel				
6.10	Closure head nut	Surfaces	Visual, VT-1	Article RIM-3 (VII-1.4.6, VII-3.4.6)
6.20	Closure studs [Note (1)]	IWB-2500-12(a)	Volumetric [Note (2)]	Article RIM-3 (VII-1.4.4, VII-3.4.4)
6.40	Threads in flange	IWB-2500-12(a)	Volumetric	Article RIM-3 (VII-1.4.4, VII-3.4.4)
6.50	Closure washers	Surfaces	Visual, VT-1	Article RIM-3 (VII-1.4.6, VII-3.4.6)
Pressurizer				
6.60	Bolts and studs [Note (1)]	IWB-2500-12(a)	Volumetric [Note (2)]	Article RIM-3 (VII-1.4.4, VII-3.4.4)
6.70	Flange surfaces [Note (3)], when connection disassembled	Surfaces	Visual, VT-1	Article RIM-3 (VII-1.4.6, VII-3.4.6)
6.80	Nuts, bushings, and washers	Surfaces	Visual, VT-1	Article RIM-3 (VII-1.4.6, VII-3.4.6)
Steam Generators				
6.90	Bolts and studs [Note (1)]	IWB-2500-12(a)	Volumetric [Note (2)]	Article RIM-3 (VII-1.4.4, VII-3.4.4)
6.100	Flange surfaces [Note (3)], when connection disassembled	Surfaces	Visual, VT-1	Article RIM-3 (VII-1.4.6, VII-3.4.6)
6.110	Nuts, bushings, and washers	Surfaces	Visual, VT-1	Article RIM-3 (VII-1.4.6, VII-3.4.6)
Heat Exchangers				
6.120	Bolts and studs [Note (1)]	IWB-2500-12(a)	Volumetric [Note (2)]	Article RIM-3 (VII-1.4.4, VII-3.4.4)
6.130	Flange surfaces [Note (3)], when connection disassembled	Surfaces	Visual, VT-1	Article RIM-3 (VII-1.4.6, VII-3.4.6)
6.140	Nuts, bushings, and Washers	Surfaces	Visual, VT-1	Article RIM-3 (VII-1.4.6, VII-3.4.6)
Piping				
6.150	Bolts and studs [Note (1)]	IWB-2500-12(a)	Volumetric [Note (2)]	Article RIM-3 (VII-1.4.4, VII-3.4.4)
6.160	Flange surfaces [Note (3)], when connection disassembled	Surfaces	Visual, VT-1	Article RIM-3 (VII-1.4.6, VII-3.4.6)
6.170	Nuts, bushings, and washers	Surfaces	Visual, VT-1	Article RIM-3 (VII-1.4.6, VII-3.4.6)
Pumps				
6.180	Bolts and studs [Note (1)]	IWB-2500-12(a)	Volumetric [Note (2)]	Article RIM-3 (VII-1.4.4, VII-3.4.4)
6.190	Flange surfaces [Note (3)], when connection disassembled	Surfaces	Visual, VT-1	Article RIM-3 (VII-1.4.6, VII-3.4.6)
6.200	Nuts, bushings, and washers	Surfaces	Visual, VT-1	Article RIM-3 (VII-1.4.6, VII-3.4.6)
Valves				
6.210	Bolts and studs [Note (1)]	IWB-2500-12(a)	Volumetric [Note (2)]	Article RIM-3 (VII-1.4.4, VII-3.4.4)
6.220	Flange surfaces [Note (3)], when connection disassembled	Surfaces	Visual, VT-1	Article RIM-3 (VII-1.4.6, VII-3.4.6)
6.230	Nuts, bushings, and washers	Surfaces	Visual, VT-1	Article RIM-3 (VII-1.4.6, VII-3.4.6)
Turbine				
6.240	Bolts and studs [Note (1)]	IWB-2500-12(a)	Volumetric [Note (2)]	Article RIM-3 (VII-1.4.4, VII-3.4.4)
6.250	Flange surfaces [Note (3)], when connection disassembled	Surfaces	Visual, VT-1	Article RIM-3 (VII-1.4.6, VII-3.4.6)
6.260	Nuts, bushings, and washers	Surfaces	Visual, VT-2	Article RIM-3 (VII-1.4.6, VII-3.4.6)
Compressor				
6.270	Bolts and studs [Note (1)]	IWB-2500-12(a)	Volumetric [Note (2)]	Article RIM-3 (VII-1.4.4, VII-3.4.4)
6.280	Flange surfaces [Note (3)], when connection disassembled	Surfaces	Visual, VT-1	Article RIM-3 (VII-1.4.6, VII-3.4.6)
6.290	Nuts, bushings, and washers	Surfaces	Visual, VT-2	Article RIM-3 (VII-1.4.6, VII-3.4.6)

NOTES:

- (1) Bolting may be examined
- (a) in place under tension
 - (b) when the connection is disassembled
 - (c) when bolting is removed

Table V-1.1-5 Examination Category G-1, Pressure-Retaining Bolting Greater Than 2 in. (50 mm) in Diameter (Cont'd)

NOTES: (Cont'd)

(2) When bolts or studs are removed for examination, surface examination meeting the acceptance standards of VII-1.4.4 or VII-3.4.4 may be substituted for volumetric examination.

(3) Examination includes 1 in. (25 mm) annular surface of flange surrounding each stud.

Table V-1.1-6 Examination Category G-2, Pressure-Retaining Bolting 2 in. (50 mm) or Less in Diameter

Item No.	Parts Examined [Note (1)]	Examination Requirements/ Figure No.	Examination Method	Acceptance Standard
Reactor Vessel				
7.10	Bolts, studs, and nuts	Surface	Visual, VT-1	Article RIM-3 (VII-1.4.6, VII-3.4.6)
Pressurizer				
7.20	Bolts, studs, and nuts	Surface	Visual, VT-1	Article RIM-3 (VII-1.4.6, VII-3.4.6)
Steam Generators				
7.30	Bolts, studs, and nuts	Surface	Visual, VT-1	Article RIM-3 (VII-1.4.6, VII-3.4.6)
Heat Exchangers				
7.40	Bolts, studs, and nuts	Surface	Visual, VT-1	Article RIM-3 (VII-1.4.6, VII-3.4.6)
Piping				
7.50	Bolts, studs, and nuts	Surface	Visual, VT-1	Article RIM-3 (VII-1.4.6, VII-3.4.6)
Pumps				
7.60	Bolts, studs, and nuts	Surface	Visual, VT-1	Article RIM-3 (VII-1.4.6, VII-3.4.6)
Valves				
7.70	Bolts, studs, and nuts	Surface	Visual, VT-1	Article RIM-3 (VII-1.4.6, VII-3.4.6)
Turbine				
7.80	Bolts, studs, and nuts	Surface	Visual, VT-1	Article RIM-3 (VII-1.4.6, VII-3.4.6)
Compressor				
7.90	Bolts, studs, and nuts	Surface	Visual, VT-1	Article RIM-3 (VII-1.4.6, VII-3.4.6)

NOTE: (1) Bolting is required to be examined only when a connection is disassembled or bolting is removed.

Table V-1.1-7 Examination Category J, Pressure-Retaining Welds in Piping

Item No.	Parts Examined	Examination Requirements/ Figure No.	Examination Method	Acceptance Standard
9.10	NPS 4 or larger (DN 100)			
9.11	Circumferential welds	IWB-2500-8	Surface and volumetric [Notes (1)–(3)]	Article RIM-3 (VII-1.4.3, VII-3.4.3)
9.20	Less than NPS 4 (DN 100)			
9.21	Circumferential welds other than PWR high-pressure safety-injection system	IWB-2500-8	Volumetric or surface [Note (1)]	Article RIM-3 (VII-1.4.3, VII-3.4.3)
9.22	Circumferential welds of PWR high-pressure safety-injection system	IWB-2500-8	Volumetric [Notes (2) and (3)]	Article RIM-3 (VII-1.4.3, VII-3.4.3)
9.30	Branch pipe connection welds			
9.31	NPS 4 or larger (DN 100)	IWB-2500-9, IWB-2500-10, and IWB-2500-11	Surface and volumetric [Notes (1)–(3)]	Article RIM-3 (VII-1.4.3, VII-3.4.3)
9.32	Less than NPS 4 (DN 100)	IWB-2500-9, IWB-2500-10, and IWB-2500-11	Volumetric or surface [Note (1)]	Article RIM-3 (VII-1.4.3, VII-3.4.3)
9.40	Socket welds	IWB-2500-8	Volumetric or surface	Article RIM-3 (VII-1.4.3, VII-3.4.3)

NOTES:

- (1) For circumferential welds with intersecting longitudinal welds, surface examination of the longitudinal piping welds is required for those portions of the welds within the examination boundaries of intersecting Examination Category F and J circumferential welds.
- (2) For circumferential welds with intersecting longitudinal welds, volumetric examination of the longitudinal piping welds is required for those portions of the welds within the examination boundaries of intersecting Examination Category F and J circumferential welds. The following requirements shall also be met:
 - (a) When longitudinal welds are specified and locations are known, examination requirements shall be met for both transverse and parallel flaws at the intersection of the welds and for that length of longitudinal weld within the circumferential weld examination volume.
 - (b) When longitudinal welds are specified but locations are unknown, or the existence of longitudinal welds is uncertain, the examination requirements shall be met for both transverse and parallel flaws within the entire examination volume of intersecting circumferential welds.
- (3) For welds in carbon or low alloy steels, only those welds showing reportable preservice transverse indications need to be examined by the ultrasonic method for reflectors transverse to the weld length direction except that circumferential welds with intersecting longitudinal welds shall meet Note (2).

Table V-1.1-8 Examination Category K, Welded Attachments for Vessels, Piping, Rotating Equipment, and Valves

Item No.	Parts Examined [Note (1)]	Examination Requirements/ Figure No.	Examination Method	Acceptance Standard
Pressure Vessels				
10.10	Welded attachments	IWB-2500-13, IWB-2500-14, and IWB-2500-15	Surface [Note (2)]	Article RIM-3 (VII-1.4.5, VII-3.4.5)
Piping				
10.20	Welded attachments	IWB-2500-13, IWB-2500-14, and IWB-2500-15	Surface	Article RIM-3 (VII-1.4.5, VII-3.4.5)
Pumps				
10.30	Welded attachments	IWB-2500-13, IWB-2500-14, and IWB-2500-15	Surface	Article RIM-3 (VII-1.4.5, VII-3.4.5)
Valves				
10.40	Welded attachments	IWB-2500-13, IWB-2500-14, and IWB-2500-15	Surface	Article RIM-3 (VII-1.4.5, VII-3.4.5)
Rotating Equipment (Turbines and Compressors)				
10.50	Welded attachments	IWB-2500-13, IWB-2500-14, and IWB-2500-15	Surface	Article RIM-3 (VII-1.4.5, VII-3.4.5)

NOTES:

- (1) Weld buildup on nozzles that is in compression under normal conditions and provides only component support is excluded from examination. Examination is limited to those welded attachments that meet the following conditions:
 - (a) The attachment is on the outside surface of the pressure-retaining component.
 - (b) The attachment provides component support as defined in Section III, Division 1, Subsection NF, NF-1110.
 - (c) The attachment weld joins the attachment either directly to the surface of the component or to an integrally cast or forged attachment to the component.
 - (d) The attachment weld is full penetration, fillet, or partial penetration, either continuous or intermittent.
- (2) For the configurations shown in Division 1, Figures IWB-2500-13 and IWB-2500-14, a surface examination from an accessible side of the attachment weld shall be performed. Alternatively, for the configuration shown in Figure IWB-2500-14, a volumetric examination of volume A-B-C-D from an accessible side of the attachment weld may be performed in lieu of the examination of surfaces A-B or C-D.

Table V-1.1-9 Examination Category L-2, Pump Casings; Examination Category M-2, Valve Bodies

Item No.	Parts Examined [Note (1)]	Examination Requirements/Figure No.	Examination Method	Acceptance Standard
Pumps				
12.20	Pump casing (L-2)	Internal surfaces [Notes (1) and (2)]	Visual VT-3	Article RIM-3 (VII-1.4.7, VII-3.4.7)
Valves				
12.50	Valve body exceeding NPS 4 (DN 100) (M-2)	Internal surfaces [Notes (2) and (3)]	Visual VT-3	Article RIM-3 (VII-1.4.7, VII-3.4.7)

NOTES:

- (1) Examinations are limited to at least one pump in each group of pumps performing similar functions in the system (e.g., recirculating coolant pumps).
- (2) Examination is required only when a pump or valve is disassembled for maintenance, or repair. Examination of the internal pressure boundary shall include the internal pressure-retaining surfaces made accessible for examination by disassembly. If a partial examination is performed and a subsequent disassembly of that pump or valve allows a more extensive examination, an examination shall be performed during the subsequent disassembly. A complete examination is required only once during the interval.
- (3) Examinations are limited to at least one valve within each group of valves that are of the same size, constructional design (such as globe, gate, or check valves), and manufacturing method, and that perform similar functions in the system (such as containment isolation and system overpressure protection).

Table V-1.1-10 Examination Category N-1, Interior of Reactor Vessels; Examination Category N-2, Welded Core Support Structures and Interior Attachments to Reactor Vessels; Examination Category N-3, Removable Core Support Structures

Item No.	Parts Examined	Examination Requirements/Figure No.	Examination Method	Acceptance Standard
Reactor Vessel (BWR)				
13.20	Interior attachments within beltline region (N-2)	Accessible welds	Visual, VT-1	Article RIM-3 (VII-1.4.7, VII-3.4.7)
13.30	Interior attachments beyond beltline region (N-2)	Accessible welds	Visual, VT-3	Article RIM-3 (VII-1.4.7, VII-3.4.7)
13.40	Core support structure (N-2)	Accessible surfaces	Visual, VT-3	Article RIM-3 (VII-1.4.7, VII-3.4.7)
Reactor Vessel (PWR)				
13.50	Interior attachments within beltline region (N-2)	Accessible welds	Visual, VT-1	Article RIM-3 (VII-1.4.7, VII-3.4.7)
13.60	Interior attachments beyond beltline region (N-2)	Accessible welds	Visual, VT-3	Article RIM-3 (VII-1.4.7, VII-3.4.7)
13.70	Core support structure (N-3) [Note (1)]	Accessible surfaces	Visual, VT-3	Article RIM-3 (VII-1.4.7, VII-3.4.7)

NOTE: (1) The structure shall be removed from the reactor vessel for examination.

Table V-1.1-11 Examination Category O, Pressure-Retaining Welds in Control Rod Drive and Instrument Nozzle Housings

Item No.	Parts Examined	Examination Requirements/Figure No.	Examination Method	Acceptance Standard
Reactor Vessel (BWR)				
14.10	Welds in control rod drive (CRD) housings	IWB-2500-18	Volumetric or surface	Article RIM-3 (VII-1.4.10, VII-3.4.10)
Reactor Vessel (PWR)				
14.20	Welds in control rod drive (CRD) housings	IWB-2500-18	Volumetric or surface [Note (1)]	Article RIM-3 (VII-1.4.10, VII-3.4.10)
14.21	Welds in in-core instrumentation nozzle (ICI) housings > NPS 2 (DN 50)	IWB-2500-18	Volumetric or surface [Note (1)]	Article RIM-3 (VII-1.4.10, VII-3.4.10)

NOTE: (1) The surface examination method shall be performed on the inside diameter of the penetration nozzle housing welds as shown in Division 1, Figure IWB-2500-18 for examination surface area C-D.

Table V-1.1-12 Examination Category P, All Pressure-Retaining Components

Item No.	Parts Examined	Examination Requirements/Figure No.	Examination Method	Acceptance Standard
15.10	Pressure-retaining components	System leakage test	Visual, VT-2	Article RIM-3 (VII-1.4.9, VII-3.4.9)
15.20	Pressure-retaining components	System leakage test	Visual, VT-2	Article RIM-3 (VII-1.4.9, VII-3.4.9)

NOTE: (1) VT-2 visual examination of Division 1, IWA-5240.

Table V-1.1-13 Examination Category F-A, Supports

Item No.	Parts Examined	Examination Requirements		
		[Notes (1), (2)]/Figure No.	Examination Method	Acceptance Standard
F1.10 [Note (3)]	Piping supports	IWF-1300-1	Visual, VT-3	Article RIM-3 (VII-1.4.11, VII-3.4.11)
F1.40	Supports other than piping supports	IWF-1300-1	Visual, VT-3	Article RIM-3 (VII-1.4.11, VII-3.4.11)

NOTES:

- (1) Examination may be limited to portions of supports that are accessible for examination without disassembly or removal of support members.
- (2) To the extent practical, the same supports selected for examination during the first inspection interval shall be examined during each successive inspection interval.
- (3) Item numbers shall be categorized to identify support types by component support function (e.g., A = supports such as one directional rod hangers; B = supports such as multidirectional restraints; and C = supports that allow thermal movement, such as springs).

MANDATORY APPENDIX VI

RELIABILITY AND INTEGRITY MANAGEMENT

EXPERT PANEL (RIMEP)

ARTICLE VI-1

OVERVIEW

VI-1.1 RESPONSIBILITIES AND QUALIFICATIONS OF RIMEP

(a) The RIMEP shall oversee the following:

(1) development, documentation, and implementation of a RIM Program, designed to achieve Reliability Targets, in accordance with [Article RIM-2](#)

(2) performance of the evaluations for Alternative Requirements per [Nonmandatory Appendix A](#)

(3) formation of the MANDEEP, in accordance with [Mandatory Appendix IV, IV-1.3.2](#)

(b) The RIMEP will identify the RIM Program scope, the associated plant and SSC Reliability Targets, and candidate RIM strategies, accounting for uncertainty in predicting SSC reliability performance.

(c) The RIMEP will document and implement the RIM strategies, MANDE methods specified by the MANDEEP program performance monitoring, and update plans.

(d) The work of the RIMEP will be independent from production and operational concerns and will be provided with full access to necessary data and will additionally be adequately funded and provided with reasonable time to complete its work.

(e) The RIMEP will be formed by and be responsible to the Panel Chair. The Chair will have a broad base of knowledge of power plant, system, and component reliability, as well as plant PRA methods and insights, together with a working knowledge of inspection, monitoring, operation, examination, test, and maintenance activities affecting SSC reliability. The Chair will hold a minimum of 4-yr technical degree from an accredited college or university. In addition, the Chair will have a minimum of 15 yr of experience in systems risk and reliability. It is recommended that at least 5 yr of this experience was obtained in a nuclear

power plant operating or nuclear design environment. The Chair shall be organizationally independent within the plant owner's organization. The Chair and RIMEP members may be employed by the Owner but shall have functional independence, similar to independence that is afforded to Quality Assurance functions.

(f) The initial composition of the RIMEP shall be determined by the Chair and include members with in-depth knowledge of all the relevant technical areas related to RIM for a specific nuclear power plant design including the following:

(1) PRA

(2) development of RIM Reliability Targets

(3) application of the RIM process

(4) inservice inspection and NDE

(5) SSC performance

(g) RIMEP members shall be selected based on their expertise in a given subject or discipline, which contributes to the assigned effort. RIMEP membership shall be based on the individual's expertise in the subject matter and this expertise shall be documented to justify their selection.

(h) The Chair shall establish the RIMEP with membership initially based on informed assumptions as to the scope and technologies necessary to implement the RIM Program. The Chair shall prepare a document addressing the basis for RIMEP formation. The basis document shall describe staffing of the RIMEP and the work schedule and funding necessary to conduct the activities defined in the RIMEP basis document. The RIMEP basis document shall be reviewed and validated, or modified as determined by the panel formed.

MANDATORY APPENDIX VII

SUPPLEMENTS FOR TYPES OF NUCLEAR PLANTS

ARTICLE VII-1

SUPPLEMENT FOR LIGHT WATER REACTOR-TYPE PLANTS

VII-1.1 SCOPE

This Supplement shall be used to provide specific requirements to the RIM Program for the plant type (i.e., in identifying and evaluating potentially active degradation mechanisms and other unique requirements to supplement the RIM Program).

(a) This Supplement shall only be used for Generation 3 or above light water reactors.

(b) Division 1, Article IWA-3000 shall be used as reference information to support this Supplement and is referenced by this Supplement.

(c) This Supplement shall only be used when ferritic components are limited to a maximum Design Temperature of 700°F (370°C) and austenitic components are limited to a maximum Design Temperature of 800°F (426°C).

VII-1.2 RIM PROGRAM — DAMAGE DEGRADATION ASSESSMENT

See [Table VII-1.2-1](#).

VII-1.3 ACCEPTANCE STANDARDS

VII-1.3.1 Evaluation of Examination Results

VII-1.3.1.1 Preservice Volumetric and Surface Examinations

(a) *General*

(1) The preservice volumetric and surface examinations required by [RIM-2.7.3](#) and performed in accordance with [RIM-2.9](#) shall be evaluated in accordance with standards specified in (b).

(2) Acceptance of components for service shall be in accordance with (b) and (c).

(b) *Acceptance*

(1) A component whose volumetric or surface examination in accordance with [RIM-2.7.3](#) meets (-a), (-b), or (-c) shall be acceptable for service, provided the verified flaws are recorded in accordance with the requirements of [RIM-1.4\(h\)](#) and [RIM-2.9.2\(b\)](#) in terms of location, size,

shape, orientation, and distribution within the component.

(-a) The volumetric or surface examination ([RIM-2.7.3](#)) confirms the absence of flaws or identifies only flaws that have already been shown to meet the non-destructive examination standards of the Construction Code for materials or welds as applicable, documented in Quality Assurance Records.

(-b) Volumetric examination detects flaws that are confirmed by surface or volumetric examination to be non-surface-connected and that do not exceed the standards of [Table VII-1.3.3-1](#).

(-c) Volumetric examination detects flaws that are confirmed by surface or volumetric examination to be non-surface-connected and that are accepted by analytical evaluation in accordance with the provisions of [VII-1.3.1.3\(b\)\(4\)](#) to the end of the service lifetime of the component and reexamined in accordance with the requirements of [RIM-2.7.6.3\(a\)](#) and [RIM-2.7.6.3\(b\)](#).

(2) A component whose volumetric or surface examination ([RIM-2.7.3](#)) detects flaws that do not meet the criteria established in (1) shall be unacceptable for service, unless the component is corrected by a repair/replacement activity in accordance with (c) to the extent necessary to meet the provisions of (1) prior to placement of the component in service.

(3) A component whose volumetric or surface examination ([RIM-2.7.3](#)) detects flaws, other than the flaws of (2) that exceed the standards of [Table VII-1.3.3-1](#) is unacceptable for service, unless the component is corrected by a repair/replacement activity to the extent necessary to meet the acceptance standards prior to placement of the component in service.

(c) *Repair/Replacement Activity and Preservice Examination.* The repair/replacement activity and preservice examination shall comply with the requirements of [Article RIM-4](#). Preservice examination shall be conducted in accordance with the requirements of [RIM-2.9](#). The recorded results shall demonstrate that the area subjected to the repair/replacement activity meets the acceptance standards of [Table VII-1.3.3-1](#).

Table VII-1.2-1 Degradation Mechanism Attributes and Attribute Criteria (LWR)

Degradation Mechanism		Attribute Criteria	Degradation Features and Susceptible Regions	Table VII-1.3.3-1 Examination Category (as appropriate)
TF	TASCS	- Single pipe and operating temperature $>220^{\circ}\text{F}$ (104°C) and - Piping >25.4 mm (1 in.) NPS, and - Pipe segment has a slope <45 deg from horizontal (includes elbow or tee into a vertical pipe), and - Potential exists for low flow in a pipe section connected to a component allowing mixing of hot and cold fluids or - Potential exists for leakage flow past a valve (i.e., in-leakage, out-leakage, cross-leakage) allowing mixing of hot and cold fluids or - Potential exists for convection heating in dead-ended pipe sections connected to a source of hot fluid, or - Potential exists for two phase (steam/water) flow, or - Potential exists for turbulent penetration in branch pipe connected to header piping containing hot fluid with high turbulent flow, and - Calculated or measured $\Delta T > 50^{\circ}\text{F}$ (28°C), and - Richardson Number >4.0	Cracks can initiate in welds, heat affected zones (HAZ), and base metal at the pipe inner surface Affected locations can include nozzles, branch pipe connections, safe ends, and regions of stress concentration TASCS can occur over extensive portions of the pipe inner surface Crack growth is relatively slow, and through-wall cracking is not expected within an inspection period	J, K
	TT	- Operating temperature $>270^{\circ}\text{F}$ (132°C) for stainless steel, or - Operating temperature $>220^{\circ}\text{F}$ (104°C) for carbon steel, AND - Potential for relatively rapid temperature changes including: Cold fluid injection into hot pipe segment, or Hot fluid injection into cold pipe segment, AND $\Delta T > 200^{\circ}\text{F}$ (111°C) for stainless steel, or $\Delta T > 150^{\circ}\text{F}$ (83°C) for carbon steel, or $\Delta T > \Delta T$ allowable or - Allowable cycles $<10^6$		J, K
VF	FIV	- Presence of attachments in a high velocity flow field, including: Welded attachments, or Attachments with small radii at the attachment junction OR - High velocity cross flow over S/G or H/X tube bundles, and - Absence of vibration damping tube supports	Cracks can initiate in welds, HAZ, and base metal at the component inner or outer surface Affected locations can include welded attachments and regions of stress concentration Crack growth can be relatively fast, and through-wall cracks can occur within an inspection period	A, B, D, F, J, K, O
	MF	- Cyclic applied loads, and - Presence of partial penetration welds, or - Presence of small radii at the attachment junction OR - Presence of attached vibration sources (e.g., pumps, compressors) and - No preoperational vibration testing or monitoring, or - No vibratory monitoring of vibration sources during operation		B, D, F, J, K, O
	SF	- Relative sliding motion between two contacting surfaces, and - Absence of a solid lubricating system at the contacting surfaces	Cracking, pitting, spalling wear, or seizing can occur at the contact surfaces Cracking is expected to be localized and not grow through-wall	G-1, G-2, K

Table VII-1.2-1 Degradation Mechanism Attributes and Attribute Criteria (LWR) (Cont'd)

Degradation Mechanism		Attribute Criteria	Degradation Features and Susceptible Regions	Table VII-1.3.3-1 Examination Category (as appropriate)
SCC	IGSCC	- Material is austenitic stainless steel weld or HAZ and - Operating temperature $\geq 200^{\circ}\text{F}$ (93°C), and - Susceptible material (carbon content $\geq 0.035\%$), and - Oxygen or oxidizing species are present OR - Material is Alloy 82 or 182, and - Operating temperature $\geq 200^{\circ}\text{F}$ (93°C), and - Oxygen or oxidizing species are present OR - Material is austenitic stainless steel weld or HAZ, and - Operating temperature $< 200^{\circ}\text{F}$ (93°C), and - Susceptible material (carbon content $\geq 0.035\%$), and - Oxygen or oxidizing species are present, and - Initiating contaminants (e.g., thiosulfate, fluoride, chloride) are present OR - Material is in an aqueous environment, and - Oxygen or oxidizing species are present, and - Mechanically induced high residual stresses are present	Cracks can initiate in welds, and HAZ at the pipe inner surface Affected locations can include pipe welds, branch pipe connections, and safe end attachment welds, Crack growth is relatively slow, and through-wall cracking is not expected within an inspection period	A, B, D, F,G-1, G-2, J, K, O
	TGSCC	- Material is austenitic stainless steel, and - Operating temperature $> 150^{\circ}\text{F}$ (65°C), and - Halides (e.g., fluoride, chloride) are present, or - Caustic (NaOH) is present, and - Oxygen or oxidizing species are present (only required to be present in conjunction w/halides; not required w/caustic), or - components in stagnant RCS locations such as pressurizer heater bundles	Cracks can initiate in welds, HAZ, and base metal at the pipe inner surface Crack growth is relatively slow, and through-wall cracking is not expected within an inspection period	A, B, D, F,G-1, G-2, J, K, O
	ECSCC	- Material is austenitic stainless steel, and - Operating temperature $> 68^{\circ}\text{F}$ (20°C), and - An outside piping surface is within five diameters of a probable leak path (e.g., valve stems) and is covered with nonmetallic insulation that is not in compliance with USNRC Reg. Guide 1.36, or - Piping surface is exposed to wetting from chloride bearing environments (e.g., seawater, sea spray, brackish water, brine) during fabrication, storage or operation	Cracks can initiate in welds, HAZ, and base metal at the pipe outer surface ECSCC can occur over extensive portions of the pipe inner or outer surface when exposed to wetting from chloride bearing environments during fabrication, storage or operation Crack growth is relatively slow, and through-wall cracking is not expected within an inspection period	J, K
	PWSCC	- Piping material is nickel-based alloy (e.g., Alloy 690), and - Exposed to primary water at $T > 525^{\circ}\text{F}$ (274°C), and - The material is mill-annealed and cold worked, or cold worked and welded without stress relief	Cracks can initiate in welds, HAZ, and base metal at the pipe inner surface Affected locations can include welds and HAZ without stress relief, the inside surface of nozzles, and areas of stress concentration Crack growth can be relatively fast, and through-wall cracks can occur within an inspection period	F, J, K

Table VII-1.2-1 Degradation Mechanism Attributes and Attribute Criteria (LWR) (Cont'd)

Degradation Mechanism		Attribute Criteria	Degradation Features and Susceptible Regions	Table VII-1.3.3-1 Examination Category (as appropriate)
LC	MIC	- Operating temperature <150°F (66°C), and - Low or intermittent flow <8 ft/sec (2.4 m/s), and - pH <10, and - presence/intrusion of organic material (e.g., raw water systems), or - water source is not treated with biocides.	Fittings, welds, HAZ's, base metal, dissimilar metal joints (for example welds and flanges), and regions containing crevices Diesel fuel MIC can occur at diesel fuel/water interface tanks. The bacteria living in the water use fuel as food. On welded stainless steel, MIC can cause welds to "sugar". The metal crystal structure changes and resembles sugar crystals. Welding tends to segregate metals in the alloy. Metals such as iron and cobalt are more susceptible to MIC than other metals. Iron and sulfur bacteria can lead to corrosion of the interior and exterior surfaces of buried water pipes. Cooling water systems (e.g., cooling tower and circulating water system)	B, D, J, K
	PIT	- Potential exists for low fluid flow, and - oxygen or oxidizing species are present, and - initiating contaminants (e.g., fluoride or chloride) are present	Pitting can initiate in welds, HAZ, base metal at the component inner surface. Forging material used in nozzles is typically SA-508, Class 2 (UNS K12766) These materials are usually clad with austenitic stainless steel weld metal, Type 308 stainless steel, to provide improved pitting resistance during low temperature shutdown. Pitting susceptibility increases for clean surfaces (no passive layer) of Alloy 600 tubing and is a function of copper chloride concentration and temperature.	B, D, F, J, K
	CC	- crevice condition exists (that is, thermal sleeves), and - operating temperature >150°F (66°C), and - oxygen or oxidizing species are present	Since PWRs that operate in accordance with the EPRI water chemistry guidelines have deaerated environments in both the primary and secondary systems, electrochemical crevice corrosion is not usually a concern. However, it should be noted that off-chemistry oxidizing conditions could occur on the secondary side through the introduction of air-saturated makeup water or through high copper levels that could establish electrochemical crevices.	A, B, D, F, J, K, O

Table VII-1.2-1 Degradation Mechanism Attributes and Attribute Criteria (LWR) (Cont'd)

Degradation Mechanism		Attribute Criteria	Degradation Features and Susceptible Regions	Table VII-1.3.3-1 Examination Category (as appropriate)
LC (Cont'd)	CC (Cont'd)		Elevated impurity concentrations and potential gradients in a crevice can initiate stress corrosion cracking in otherwise resistant material, such as non-sensitized Type 316 stainless steel or low carbon grades Type 304L and 316L stainless steel. Surface cold work can lead to initiation and propagation of stress corrosion cracking. Annealed Types 304, 304L, and 316L stainless steel, nickel-based alloys (e.g., Inconel) as well as Alloy 600 are susceptible. During fabrication and installation of components, activities such as grinding, machining, bending, etc. can produce a thin layer of cold-worked metal surface, creating the same susceptibility to initiation as intentionally cold-worked material. Once the crack extends across the cold-work layer, the resulting crevice can provide the electrochemical driving force for continued crack propagation. Susceptible regions include CRD hydraulic return nozzle thermal sleeve (if applicable), spray nozzle thermal sleeve, and feedwater thermal sleeve. Crevice corrosion can also initiate in welds and HAZ at the component inner surface. Crack growth is relatively slow, and through-wall cracking is not expected within an inspection period.	
FS	E-C	- Existence of cavitation sources (i.e., throttling or pressure-reducing valves or orifices), and - Helium environment, and - No monitoring or control of impurities in the helium flow stream, OR - Existence of cavitation sources (i.e., throttling or pressure-reducing valves or orifices), and stream environment, and - Operating temperature <250°F (120°C), and - Flow present >100 hr/yr and - Flow velocity >30 ft/sec (9.1 m/s)	Wall thinning can initiate in welds, HAZ, and base metal at the component inner surface. Affected locations can include regions up to one or two pipe diameters downstream of the cavitation source. Degradation growth is relatively slow, and through-wall degradation is not expected within an inspection period.	B, J
	FAC	- Carbon or low alloy steel piping with Cr <0.5% (some literature indicates 0.1%) and - Wet steam environment (i.e., two-phase flow) or	Wall thinning can initiate in welds, HAZ, and base metal at the component inner surface.	A, B, D, F, J, O

Table VII-1.2-1 Degradation Mechanism Attributes and Attribute Criteria (LWR) (Cont'd)

Degradation Mechanism		Attribute Criteria	Degradation Features and Susceptible Regions	Table VII-1.3.3-1 Examination Category (as appropriate)
FS (Cont'd)	FAC (Cont'd)	- Any high-purity water environment coupled with - Low levels of dissolved oxygen - And flow (there is no known practical threshold velocity below which FAC will not occur) [reference: T. M. Laronge, M. A. Ward, "The Basics and Not so Basics of Water Corrosion Processes Altered by Flow Changes," CORROSION/99, paper 99345, NACE International, Houston, TX (1999)] - Accelerated further by turns in the flow path and - Low or very high pH - Fluid flow present >100 hr/yr	affected locations can include regions where the potential for FAC degradation has been identified FAC can occur over extensive portions of the component inner surface Degradation growth is relatively slow, and through-wall degradation is not expected within an inspection period	
	PE	- Solid Particle Erosion (SPE) is damage caused by particles transported by the fluid stream rather than by liquid water or collapsing bubbles. In contrast to liquid impingement erosion, the necessary velocities for SPE are low, approximately 3 ft/sec. SPE also requires the presence of particles of sufficient size, typically >0.004 in. (100 microns). - Erosion rate decreases in ductile materials rapidly with decreasing particle size below 0.004 in. (100 microns).	Wall thinning can initiate in welds, HAZ, and base metal at the component inner surface. "Hard materials" (e.g., Stellite) offered only modest improvement over carbon steel. The Inconel alloys offered only a very modest improvement over carbon steel. Unless exotic materials are used (i.e., ceramics), there is no material solution to SPE. Susceptible regions include valve internals, nozzles, and the steam turbine. Degradation growth is relatively slow, and through-wall degradation is not expected within an inspection period.	B, D, F, J
DEP	WH	- Plant/system specific history of water hammer, in piping containing water/steam, and - No corrective measures have been implemented	Increased potential pipe rupture and extension of existing flaws Affected locations include turns in the pipe run Pipe rupture or extension of existing cracks can occur instantaneously	B, J, K
	RE	- Ferritic steels with high energy (>1 MeV) neutron fluence $>10^{17}$ n/cm² - OR - Austenitic stainless steels with high energy (>1 MeV) neutron fluence $>3 \times 10^{23}$ n/cm²	Reduced fracture toughness of welds, HAZ, and base metal exposed to high levels of neutron fluence	A, B, D, F, J, O
	TA	9Cr-1Mo or other high-temperature super alloys with operating temperature >930°F (500°C)	Reduced fracture toughness of castings or welds with long term exposure to high temperature	A, B, D, F, J
	LE	Potential for degradation (deposition/scale formation, fouling, erosion) of heat transfer surface	Reduced emissivity and heat transfer with potential for inadequate cooling	B
SP [Note(1)]	LP	Potential for debris from, failed components/materials to migrate into the high energy primary coolant flow stream	Susceptible areas include core cooling channels	A, B, J, O

Table VII-1.2-1 Degradation Mechanism Attributes and Attribute Criteria (LWR) (Cont'd)

Degradation Mechanism		Attribute Criteria	Degradation Features and Susceptible Regions	Table VII-1.3.3-1 Examination Category (as appropriate)
SP (Cont'd)	RIA [Note (1)]	– Component is inaccessible for conventional volumetric or visual inspection	Applicable areas include: Regions with little or no physical access, Environments hazardous to personnel, Cost/benefit of inservice inspection is prohibitive to relative to plant reliability goals	A, B, D, F, G-1, G-2, J, K, O

Legend:

CC = crevice corrosion
DEP = degradation enhancement phenomena
E-C = erosion-cavitation
ECSCC = external chloride stress corrosion cracking
FAC = flow-accelerated corrosion
FIV = flow-induced vibration
FS = flow sensitive
IGSCC = intergranular stress corrosion cracking
LE = lowered emissivity
LP = loose parts
MF = mechanical fatigue
MIC = microbiologically induced corrosion
PC = pitting corrosion
PE = particle erosion-corrosion
PWSCC = primary water stress corrosion cracking
RE = radiation embrittlement
RIA = restricted inspection access [Note (1)]
SCC = stress corrosion cracking
SF = self-welding and fretting fatigue
SP = spatial phenomena [Note (1)]
TA = thermal aging
TASCS = thermal stratification cycling and striping
TF = thermal fatigue
TGSCC = transgranular stress corrosion cracking
TT = thermal transients
VF = vibration fatigue
WH = water hammer

NOTE: (1) RIA and SP are not degradation mechanisms but must be considered in the development or application of MANDE criteria established by MANDEEP.

VII-1.3.1.2 Preservice Visual Examinations

(a) General

(1) The preservice visual examinations required by RIM-2.7.3 and performed in accordance with RIM-2.9 shall receive an NDE evaluation by comparing the examination results with the acceptance standards specified in Table VII-1.3.3-1.

(2) Acceptance of components for service shall be in accordance with (b) and (c).

(b) Acceptance

(1) Acceptance by Visual Examination

(-a) A component whose visual examination confirms the absence of the relevant conditions described in the standards of Table VII-1.3.3-1 shall be acceptable for service.

(-b) A component whose visual examination detects the relevant conditions described in the standards of Table VII-1.3.3-1 shall be unacceptable for service, unless such components meet the requirements of (2) or (3) prior to placement of the component in service.

(2) *Acceptance by Supplemental Examination.* A component containing relevant conditions shall be acceptable for service if the results of supplemental examinations (VII-1.3.2) meet the requirements of VII-1.3.1.1.

(3) *Acceptance by Corrective Measures or Repair/Replacement Activity.* A component containing relevant conditions is acceptable for service if the relevant conditions are corrected by a repair/replacement activity or by

corrective measures to the extent necessary to meet the acceptance standards of [Table VII-1.3.3-1](#).

(c) *Repair/Replacement Activity and Preservice Examination.* The repair/replacement activity and preservice examination shall comply with the requirements of [Article RIM-4](#). Preservice examination shall be conducted in accordance with the requirements of [RIM-2.9](#). The recorded results shall demonstrate that the area subjected to the repair/replacement activity meets the acceptance standards of [Table VII-1.3.3-1](#).

VII-1.3.1.3 Inservice Volumetric and Surface Examinations

(a) General

(1) The volumetric and surface examinations required by [RIM-2.7.7](#) and performed in accordance with [RIM-2.9](#) shall receive an NDE evaluation by comparing the examination results with the acceptance standards specified in [Table VII-1.3.3-1](#), except where (2) is applicable.

(2) When flaws are detected by a required volumetric or surface examination, the component is acceptable for continued service provided the requirements of [VII-1.3.1.1\(b\)\(1\)](#) or the acceptance standards of [Table VII-1.3.3-1](#) are met.

(3) Volumetric and surface examination results shall be compared with recorded results of the preservice examination and prior inservice examinations. Acceptance of the components for continued service shall be in accordance with (b) and (c).

(b) Acceptance

(1) *Acceptance by Volumetric or Surface Examination.* A component whose volumetric or surface examination either reconfirms the absence of flaws or detects flaws that are acceptable under the provisions of (a)(2) are acceptable for continued service. Confirmed changes in flaws from prior examinations shall be recorded in accordance with [RIM-1.4\(h\)](#) and [RIM-2.9.2\(b\)](#). A component that does not meet the acceptance standards of [Table VII-1.3.3-1](#) shall be corrected in accordance with the provisions of (2), (3), or (4).

(2) *Acceptance by Supplemental Examination.* A component containing flaws shall be acceptable for service if the results of supplemental examinations ([VII-1.3.2](#)) meet the requirements of [VII-1.3.1.1](#).

(3) *Acceptance by Repair/Replacement Activity.* A component whose volumetric or surface examination detects flaws that exceed the acceptance standards of [Table VII-1.3.3-1](#) is unacceptable for continued service until the component is corrected by a repair/replacement activity to the extent necessary to meet the acceptance standards of [VII-1.3](#).

(4) *Acceptance by Analytical Evaluation.* A component whose volumetric or surface examination detects flaws that exceed the acceptance standards of [Table VII-1.3.3-1](#), or for which the acceptance standards

are not applicable, is acceptable for continued service without a repair/replacement activity if an analytical evaluation, as described in [VII-1.5](#), meets the acceptance criteria of [VII-1.5](#). The area containing the flaw shall be subsequently reexamined in accordance with [RIM-2.7.6.3\(a\)](#) and [RIM-2.7.6.3\(b\)](#). If the subsequent [RIM-2.7.6.3\(a\)](#) and [RIM-2.7.6.3\(b\)](#) examinations reveal that the flaws remain essentially unchanged, or the flaw growth is within the growth predicted by the analytical evaluation, and the design inputs for the analytical evaluation have not been affected by activities such as power uprates, the existing analytical evaluation may continue to be used, provided it covers the time period until the next examination.

(c) *Repair/Replacement Activity and Reexamination.* The repair/replacement activity and reexamination shall comply with the requirements of [Article RIM-4](#). Reexamination shall be conducted in accordance with the requirements of [RIM-2.9](#). The recorded results shall demonstrate that the area subjected to the repair/replacement activity meets the acceptance standards of [Table VII-1.3.3-1](#).

VII-1.3.1.4 Inservice Visual Examinations

(a) General

(1) The visual examinations required by [RIM-2.7.7](#) and performed in accordance with [RIM-2.9.1](#) shall be evaluated by comparing the examination results with the acceptance standards specified in [Table VII-1.3.3-1](#).

(2) Acceptance of components for continued service shall be in accordance with (b).

(b) Acceptance

(1) Acceptance by Visual Examination

(-a) A component whose visual examination confirms the absence of the relevant conditions described in the standards of [Table VII-1.3.3-1](#) shall be acceptable for continued service.

(-b) A component whose visual examination detects the relevant conditions described in the standards of [Table VII-1.3.3-1](#) shall be unacceptable for continued service, unless such components meet the requirements of (2), (3), or (4).

(2) *Acceptance by Supplemental Examination.* A component containing relevant conditions shall be acceptable for continued service if the results of supplemental examinations ([VII-1.3.2](#)) meet the requirements of [VII-1.3.1.3](#).

(3) *Acceptance by Corrective Measures or Repair/Replacement Activity.* A component containing relevant conditions is acceptable for continued service if the relevant conditions are corrected by a repair/replacement activity or by corrective measures to the extent necessary to meet the acceptance standards of [Table VII-1.3.3-1](#).

(4) *Acceptance by Evaluation.* A component containing relevant conditions is acceptable for continued service if an evaluation demonstrates the component's

Table VII-1.3.3-1 Acceptance Standards

Examination Category	Component and Part Examined	Acceptance Standard
A, B	Vessel welds	VII-1.4.1
D	Full penetration welded nozzles in vessels	VII-1.4.2
F, J	Dissimilar and smaller metal welds in piping and vessel nozzles	VII-1.4.3
G-1	Bolting greater than 2 in. (50 mm) in diameter	VII-1.4.4 and VII-1.4.6
G-2	Bolting 2 in. (50 mm) in diameter and less	VII-1.4.6
K	Welded attachments for vessels, piping, pumps, and valves	VII-1.4.5
L-2, M-2	Pump casings and valve bodies	VII-1.4.7
N-1, N-2, N-3	Interior surfaces and internal components of reactor vessels	VII-1.4.8
O	Control rod drive and instrument nozzle housing welds	VII-1.4.10
P	Pressure-retaining boundary	VII-1.4.9
F-A	Piping and other supports	VII-1.4.11

acceptability. The evaluation and acceptance criteria shall be specified by the Owner. A component accepted for continued service based on evaluation shall be subsequently examined in accordance with RIM-2.7.6.3(a) and RIM-2.7.6.3(b). If the subsequent RIM-2.7.6.3(a) and RIM-2.7.6.3(b) examinations reveal that the relevant conditions remain essentially unchanged, or the changes in the relevant conditions are within the limits predicted by the evaluation, and the design inputs for the evaluation have not been affected by activities such as power uprates, the existing evaluation may continue to be used, provided it covers the time period until the next examination.

(c) *Repair/Replacement Activity and Reexamination.* The repair/replacement activity and reexamination shall comply with the requirements of Article RIM-4. Reexamination shall be conducted in accordance with the requirements of RIM-2.9. The recorded results shall demonstrate that the area subjected to the repair/replacement activity meets the acceptance standards of Table VII-1.3.3-1.

VII-1.3.2 Supplemental Examinations

(a) Volumetric or surface examinations that detect flaws that require NDE evaluation in accordance with the requirements of VII-1.3.1 may be supplemented by other examination methods and techniques (RIM-2.9.4) to determine the character of the flaw (i.e., size, shape, and orientation).

(b) Visual examinations that detect relevant conditions described in the standards of this Article may be supplemented by surface or volumetric examinations to determine the extent of the unacceptable conditions and the need for corrective measures, evaluation or repair/replacement activities.

(c) Supplemental examinations shall meet the requirements of RIM-2.9.4 and Mandatory Appendix IV.

VII-1.3.3 Acceptance Standards

The acceptance standards referenced in Table VII-1.3.3-1 shall be applied to determine acceptability for service. The conditions in VII-1.3.3.1 and VII-1.3.3.2 shall apply.

VII-1.3.3.1 Application of Standards

(a) The acceptance standards for ferritic steel components shall only be applicable to those components whose material properties are in accordance with those stated in the referenced table.

(b) The acceptance standards for ferritic steel components shall be applicable where the maximum postulated defect that determines the limiting operating conditions conforms to the recommendations stated in Section III, Division I, Appendices.

VII-1.3.3.2 Modification of Standards

(a) Where less than the maximum postulated defect is used, as permitted by Section XI, Division 1, Nonmandatory Appendix G, or operating conditions are modified from those originally assumed, the acceptance standards of this Article shall be modified.

(b) The Owner shall be responsible for modification of acceptance standards as necessary to maintain the equivalent structural factors¹ of the acceptance standards of this Article.

(c) Modified standards shall not allow greater flaw sizes than those contained in this Article for the applicable examination category.

VII-1.3.4 Characterization

Each detected flaw or group of flaws shall be characterized by the requirements of Division 1, IWA-3300 to establish the dimensions of the flaws. These dimensions shall be used in conjunction with the acceptance standards of VII-1.4.

VII-1.3.5 Acceptability

(a) Flaws that do not exceed the dimensions of allowable flaws of VII-1.4 for the respective examination category shall be acceptable, unless such flaws are in UNS N06600, N06082, or W86182 environments or in austenitic stainless steels and associated welds, which are subject to stress corrosion cracking.

(b) For acceptance by analytical evaluation, planar surface flaws in the above materials shall meet the provisions of VII-1.5.

VII-1.4 ACCEPTANCE STANDARDS FOR SPECIFIC EXAMINATION CATEGORIES

VII-1.4.1 Standards for Examination Categories A and B of Pressure-Retaining Welds in Reactor Vessel and Other Vessels

VII-1.4.1.1 Allowable Planar Flaws

(a) The size of allowable planar flaws within the boundary of the examination volumes specified in Division 1, Figures IWB-2500-1 through IWB-2500-6 shall not exceed the limits specified in Division 1, Table IWB-3510-1 or Table IWC-3510-1 (based on thickness) for ferritic steels or IWB-3514-1 for austenitic steels.

(b) Where a flaw extends or lies beyond the examination volumes as detected by the procedures used to examine the specified volumes, the overall size of the flaw shall be compared with the standards specified in Division 1, Table IWB-3510-1 or Table IWC-3510-1 (based on thickness) for ferritic steels or Division 1, Table IWB-3514-1 for austenitic steels.

(c) Any two or more coplanar aligned flaws characterized as separate flaws by Division 1, IWA-3330 are allowable, provided the requirements of IWA-3390 are met.

(d) Surface flaws within cladding are acceptable.

VII-1.4.1.2 Allowable Laminar Flaws

(a) The areas of allowable laminar flaws as defined by Division 1, IWA-3360 within the boundary of the examination zones delineated in the applicable figures specified in VII-1.4.1.1(a) shall not exceed the limits specified in Division 1, Table IWB-3510-2.

(b) Laminar flaws that join with a planar flaw shall be governed by the standards of Division 1, Table IWB-3510-1 or Table IWC-3510-1 (based on thickness).

VII-1.4.1.3 Allowable Linear Flaws

(a) The size of allowable linear flaws as detected by a surface examination (MT/PT) or volumetric examination (RT) within the examination boundary shown in Division 1, Figures IWB-2500-1 through IWB-2500-6 shall not exceed the limits specified in Division 1, Table IWB-3510-3 for ferritic steels or Division 1, Table IWB-3514-2 for austenitic steels.

(b) Where a flaw extends beyond the examination boundaries, or separate linear flaws lie both within and beyond the boundaries but are characterized as a single flaw by Division 1, IWA-3400, the overall flaw size shall be compared with the standards of Division 1, Table IWB-3510-3 for ferritic steels or Division 1, Table IWB-3514-2 for austenitic steels.

VII-1.4.1.4 Material Requirements for Application of Acceptance Standards. The material requirements specified in this paragraph are for the acceptance standards in Table IWB-3510-1, Table IWC-3510-1, Table IWB-3510-3, Table IWB-3512-1, Table IWC-3511-1, Table IWC-3511-2, Table IWB-3514-1, Table IWB-3514-4, and Table IWB-3519.2-1 of Division 1. The acceptance standards identified in these tables are applicable to ferritic steels that satisfy one of the following conditions:

(a) Ferritic steels having specified minimum yield strength of 50 ksi (350 MPa) or less at room temperature and meeting the requirements of Section III, Subsection NB, NB-2300.

(b) The material meets one of the following:

(1) SA-508 Grade 2 Class 2 (former designation: SA-508 Class 2a) (UNS K12766 1)

(2) SA-508 Grade 3 Class 2 (former designation: SA-508 Class 3a) (UNS K12042 1)

(3) SA-533 Type A Class 2 (former designation: SA-533 Grade A Class 2) (UNS K12521)

(4) SA-533 Type B Class 2 (former designation: SA-533 Grade B Class 2) (UNS K12539 2)

(5) SA-508 Class 1 (UNS K13502)

(c) Ferritic steels having specified minimum yield strength greater than 50 ksi (350 MPa) but not exceeding 90 ksi (620 MPa) at room temperature shall meet the requirements of Section III, Subsection NB, NB-2300, or Subsection NC, NC-2300, and Section III Appendices, Nonmandatory Appendix G, G-2110(b). The acceptance standards may also be applied to materials with dynamic fracture toughness data K_{Ic} that exceeds the values of K_{Ic} in Section III Appendices, Nonmandatory Appendix G prior to the 1999 Addenda, or K_{Ic} in Section III Appendices, Nonmandatory Appendix G prior to the 2007 Edition.

VII-1.4.2 Standards for Examination Category D for Full Penetration Welds of Nozzles in Vessels

VII-1.4.2.1 Allowable Planar Flaws

(a) The size of allowable planar flaws detected in the nozzle and weld areas within the boundary of the examination volume specified in Division 1, Figures IWB-2500-7(a) through IWB-2500-7(d) shall not exceed the limits specified in Division 1, Table IWB-3512-1 or Table IWC-3511-1 (based on thickness) for ferritic steels or Division 1, Table IWB-3514-1 for austenitic steels.

(b) The size of allowable planar flaws detected in the vessel shell (or head) material adjoining the nozzle and weld areas and within the boundary of the examination volumes specified in Figures IWB-2500-7(a) through IWB-2500-7(d) shall not exceed the limits of Division 1, Table IWB-3510-1 or Table IWC-3510-1 (based on thickness) for ferritic steels or Table IWB-3514-1 for austenitic steels.

(c) The component thickness t to be applied in calculating the flaw a/t ratio for comparison with the standards in Division 1, Table IWB-3510-1, Table IWC-3510-1, Table IWB-3512-1 or Table IWC-3511-1, as applicable, shall be selected as specified in Division 1, Table IWB-3512-2. This table lists the component thicknesses as a function of flaw location for each type nozzle configuration as shown in Division 1, Figures IWB-2500-7(a) through IWB-2500-7(d).

(d) Any two or more coplanar aligned flaws characterized as separate flaws by Division 1, IWA-3300 are allowable, provided the requirements of IWA-3390 are met.

VII-1.4.2.2 Allowable Laminar Flaws

(a) Laminar flaws in vessel shell or head material within the boundary of the examination volumes specified in Figures IWB-2500-7(a) through IWB-2500-7(d) shall be governed by the standards of VII-1.4.1.2.

(b) Laminar flaws in the nozzle wall shall be considered as planar flaws and the standards of VII-1.4.2.1 shall apply.

VII-1.4.2.3 Allowable Linear Flaws

(a) The size of allowable linear flaws as detected by a surface examination (MT/PT) or volumetric examination (RT) within the examination boundary shown in (reference Figures IWC-2500-1 and IWC-2500-2) shall not exceed the limits specified in Division 1, Table IWC-3511-2 for ferritic steels or Division 1, Table IWB-3514-2 for austenitic steels.

(b) Where a flaw extends beyond the examination boundaries, or separate linear flaws lie both within and beyond the boundaries but are characterized as a single flaw by Division 1, IWA-3400, the overall flaw size shall be compared with the standards of Division 1, Table IWC-3511-2 ferritic steels or Table IWB-3514-2 for austenitic steels.

VII-1.4.3 Standards for Examination Category F for Pressure-Retaining Dissimilar Metal Welds in Vessel Nozzles and Category J for Pressure-Retaining Welds in Piping

(a) The acceptance standards of VII-1.4.3 do not apply to planar surface-connected flaws that are in contact with the reactor coolant environment during normal operation and are detected by inservice examination in the following materials:

(1) for PWRs, UNS N06600, N06082, or W86182 surfaces with a normal operating temperature greater than or equal to 525°F (275°C) and in contact with the reactor coolant environment

(2) for BWRs, UNS N06600, W86182, or austenitic stainless steel and associated weld surfaces in contact with the reactor coolant environment that are susceptible to stress corrosion cracking and not mitigated

(b) If the acceptance standards are not met or are not applicable, for acceptance by analytical evaluation, the planar surface-connected flaws in (a) shall meet the provisions of VII-1.5.

(c) Susceptible materials and mitigation criteria for BWRs are specified in NUREG 0313 Revision 2, Sections 2.1 and 2.2.

(d) Susceptible materials and mitigation criteria for butt welds in PWRs are specified in NUREG/CR 7187, Sections 1 and 2.3.

VII-1.4.3.1 Allowable Planar Flaws

(a) The size of allowable planar flaws within the boundary of the examination surfaces and volumes delineated in Division 1, Figures IWB-2500-8 through IWB-2500-11 shall be in accordance with the standards of VII-1.4.3.2, VII-1.4.3.3, and VII-1.4.3.4, as applicable. In addition, the requirements of Division 1, IWB-3514.8 shall be satisfied for planar surface-connected flaws that are in contact with the reactor coolant environment during normal operation and are detected by preservice examination in materials that are susceptible to stress corrosion cracking, as defined for PWRs in VII-1.4.3(a)(1) and for BWRs in VII-1.4.3(a)(2) and VII-1.4.3(c).

(b) Where flaws extend beyond the boundaries of the examination surfaces and volumes, or separate flaws are detected that lie both within and beyond the boundaries but are characterized as a single flaw by the requirements of Division 1, IWA-3300, the overall flaw size shall be compared with the standards of (a).

(c) Any two or more coplanar aligned flaws that are characterized as separate flaws by Division 1, IWA-3300 are allowable, provided the requirements of IWA-3390 are met.

(d) Inner surface flaws detected by volumetric examination of piping components with austenitic cladding on the inner surface shall be governed by the following standards:

(1) Surface flaws that do not penetrate through the nominal clad thickness into base metal need not be compared with the standards of (a).

(2) The size of allowable surface flaws that penetrate through the cladding into base metal shall not exceed the standards of (a), except that the depth of the flaw shall be the total depth minus the nominal clad thickness.

VII-1.4.3.2 Allowable Flaw Standards for Ferritic Piping

(a) The size of allowable flaws shall not exceed the limits specified in Division 1, Table IWB-3514-1.

(b) Where flaws on the outer surface of piping as detected by the surface examination method during an inservice examination exceed the allowable standards of VII-1.4.3.6, the flaws may be examined by the volumetric method. The acceptance of these flaws shall be governed by the allowable flaw standards for the volumetric examination method in Division 1, Table IWB-3514-1.

VII-1.4.3.3 Allowable Flaw Standards for Austenitic Piping

(a) The size of allowable flaws shall not exceed the limits specified in Division 1, Table IWB-3514-1.

(b) Where flaws on the outer surface of piping as detected by the surface examination method during an inservice examination exceed the allowable standards of VII-1.4.3.6, the flaws may be examined by the volumetric method. The acceptance of these flaws shall be governed by the allowable flaw standards for the volumetric examination method in Division 1, Table IWB-3514-1.

VII-1.4.3.4 Allowable Flaw Standards for Dissimilar Metal Welds

(a) The size of allowable flaws in the carbon or low alloy steel end of a dissimilar metal weld joint shall be governed by the standards of VII-1.4.3.2.

(b) The size of allowable flaws in the high alloy steel or high nickel alloy end and the weld metal of a dissimilar metal weld joint shall be governed by the standards of VII-1.4.3.3.

VII-1.4.3.5 Allowable Laminar Flaws. The area of allowable laminar flaws, as defined by Division 1, IWA-3360, within the boundary of the examination zones shown in Figure IWB-2500-8 through Figure IWB-2500-11, shall not exceed the limits specified in Division 1, Table IWB-3514-3.

VII-1.4.3.6 Allowable Linear Flaw Standards for Ferritic Piping and Austenitic Piping

(a) The size of an allowable linear flaw within the boundaries of the examination surfaces in Figures IWB-2500-8 through IWB-2500-11 shall not exceed the limits specified for ferritic piping in Table IWB-3514-4 and for austenitic piping in Table IWB-3514-2 as contained in Division 1.

(b) Where a flaw extends beyond the boundaries of the examination surfaces in Figures IWB-2500-8 through IWB-2500-11, or where discontinuous linear flaws lie both within and beyond the boundaries and are characterized as a single flaw by the requirements of IWA-3400,

the size of allowable overall linear flaws shall not exceed the limits specified for ferritic piping in Table IWB-3514-4 and for austenitic piping in Table IWB-3514-2 as contained in Division 1.

VII-1.4.4 Standards for Examination Category G-1 for Pressure-Retaining Bolting Greater Than 2 in. (50 mm) in Diameter

VII-1.4.4.1 Allowable Flaws for Surface Examinations of Studs and Bolts. Allowable surface flaws in vessel closure studs and pressure-retaining bolting shall not exceed the following limits:

- (a) non-axial flaws, $\frac{1}{4}$ in. (6 mm) in length
- (b) axial flaws, 1 in. (25 mm) in length

VII-1.4.4.2 Allowable Flaws for Volumetric Examinations of Studs and Bolts

(a) The size of allowable non-axial flaws in vessel closure studs and pressure-retaining bolting within the boundary of the examination volume shown in Figure IWB-2500-12(a) shall not exceed the limits specified in Table IWB-3515-1, which are contained in Division 1.

(b) Any two or more subsurface flaws at any diameter of the stud that combine to reduce the net diameter are acceptable, provided the combined flaw depths do not exceed the sum of the allowable limits specified in Division 1, Table IWB-3515-1 for the corresponding flaw aspect ratios, divided by the number of flaws.

(c) Any flaw detected by the volumetric examination shall be investigated by a surface examination. If confirmed to be a surface flaw, the standards of VII-1.4.4.1 shall apply. If not a surface flaw, the standards of (a) and (b) shall apply.

VII-1.4.4.3 Allowable Flaws for Volumetric Examinations of Threads in Stud Holes. The size of allowable flaws within the boundary of the examination volume in Division 1, Figure IWB-2500-12(a) and oriented on a plane normal to the axis of the stud shall not exceed 0.2 in. (5 mm) as measured radially from the root of the thread.

VII-1.4.5 Standards for Examination Category K for Welded Attachments for Vessels, Piping, Pumps, and Valves

VII-1.4.5.1 Allowable Planar Flaws

(a) The size of an allowable flaw within the boundary of the examination surfaces and volumes in Division 1, Figures IWB-2500-13, IWB-2500-14, and IWB-2500-15 shall not exceed the allowable flaw standards of this Article for the applicable supported pressure-retaining component to which the attachment is welded. For indications located wholly on the attachment side of the line A-D in Figures IWB-2500-13, IWB-2500-14, and IWB-2500-15, the thickness and the surface of the attachment shall be considered the thickness and surface of the

component for purposes of flaw indication characterization (IWA-3300) and for comparison with the allowable indication standards. For indications located in the examination volume A-B-C-D, the indication shall be characterized considering both the surface of the attachment and the surface of the pressure boundary as the surface of the component for comparison with the allowable indication standards.

(b) Where a flaw extends beyond the boundaries of the examination surfaces and volumes, or separate flaws are detected that lie both within and beyond the boundaries but are characterized as single flaws by the requirements of Division 1, IWA-3000, the overall flaw size shall be compared with the standards of (a).

(c) Where a flaw detected by a surface examination method exceeds the allowable standards of (a), an optional encoded volumetric examination may be conducted, in which case the allowable flaw standards for the volumetric examination method shall apply.

VII-1.4.5.2 Allowable Laminar Flaws

(a) The allowable area of a laminar flaw within the boundary of the examination volume of the attachment or the pressure-retaining membrane to which the support is attached shall be governed by VII-1.4.1 or VII-1.4.3, as applicable.

(b) Where laminar flaws are detected in an attachment that does not transmit tensile load in the through-thickness direction, the laminar flaw standards need not apply.

VII-1.4.5.3 Allowable Linear Flaws

(a) The size of an allowable flaw within the boundary of the examination surfaces in Division 1, Figure IWC-2500-5 shall not exceed the allowable flaw standards of this Article for the applicable supported pressure-retaining component to which the attachment is welded.

(b) Where a flaw extends beyond the boundaries of the examination surfaces, or separate flaws are detected that lie both within and beyond the boundaries but are characterized as a single flaw by the requirements of Division 1, Article IWA-3000, the overall flaw size shall be compared with the standards of (a).

(c) Where a flaw detected by a surface examination method exceeds the allowable standards of (a), an optional volumetric examination may be conducted, in which case the allowable flaw standards for the volumetric examination method for the applicable supported pressure-retaining component to which the attachment is welded shall apply.

VII-1.4.6 Standards for Examination Category G-1 for Pressure-Retaining Bolting Greater Than 2 in. (50 mm) in Diameter and G-2 for Pressure-Retaining Bolting 2 in. (50 mm) and Less in Diameter

VII-1.4.6.1 Visual Examination, VT-1. This requirement applies to accessible surfaces of bolting when examined in place and to all surfaces when bolting is removed for examination. The following relevant conditions² shall require corrective action to meet the requirements of VII-1.3.1.2(b) prior to service or VII-1.3.1.4(b) prior to continued service:

(a) crack-like flaws that exceed the allowable linear flaw standards of VII-1.4.4

(b) more than one deformed or sheared thread in the zone of thread engagement of bolts, studs, or nuts

(c) localized general corrosion that reduces the bolt or stud cross-sectional area by more than 5%

(d) bending, twisting, or deformation of bolts or studs to the extent that assembly or disassembly is impaired

(e) missing or loose bolts, studs, nuts, or washers

(f) fractured bolts, studs, or nuts

(g) degradation of protective coatings on bolting surfaces, or

(h) evidence of coolant leakage near bolting

VII-1.4.7 Standards for Examination Categories L-2 and M-2 of Rotating Equipment Casings and Valve Bodies

VIII-1.4.7.1 Visual Examination, VT-3. Relevant conditions do not include fabrication marks, material roughness, casting irregularities, and other conditions acceptable by material, design, and manufacturing specifications of the component. The following relevant conditions shall require corrective action to meet the requirements of VII-1.3.1.2(b) prior to service or VII-1.3.1.4(b) prior to continued service:

(a) corrosion or erosion that reduces the pressure-retaining wall thickness,³ determined either from design information, construction drawings, or by measurement on the component, by more than 10%

(b) wear of mating surfaces that may lead to loss of function or leakage, or

(c) crack-like surface flaws developed in service or grown in size beyond that recorded during preservice visual examination

VII-1.4.7.2 Allowable Planar Flaws. If a supplemental examination is performed that can characterize the flaw size and shape, the following acceptance standards for allowable planar flaws shall be applied:

(a) The size of an allowable planar flaw shall not exceed the limits specified in Division 1, Table IWB-3519.2-1 or Table IWB-3519.2-2, as applicable. Base metal flaws in castings that are permitted by the governing material

specifications meeting the requirements of the Construction Code are acceptable.

(b) If separate flaws are detected and are characterized as a single flaw in accordance with Division 1, IWA-3300, the flaw shall meet the requirements of (a).

(c) Any two or more coplanar aligned flaws characterized as separate flaws in accordance with IWA-3300 are acceptable, provided the requirements of Division 1, IWA-3390 are met.

(d) If a flaw is detected by radiographic examination and exceeds the allowable surface flaw standards of Division 1, Table IWB-3519.2-1 or Table IWB-3519.2-2, as applicable, surface examination may be performed, with acceptance in accordance with Division 1, Table IWB-3519.2-1 or Table IWB-3519.2-2. If acceptable by surface examination, the flaw shall meet subsurface flaw standards of Table IWB-3519.2-1 or Table IWB-3519.2-2 contained in Division 1.

(e) A surface flaw in the cladding detected by volumetric examination of austenitic clad ferritic base material shall meet the following requirements:

(1) Surface flaws that do not extend to the base material are acceptable.

(2) A surface flaw that extends into the base material shall meet the requirements of (a), considering dimension a , to be the portion of the flaw depth in the base material.

VII-1.4.8 Standards for Examination Category N-1, Interior of Reactor Vessel; Examination Category N-2, Welded Core Support Structures and Interior Attachments to Reactor Vessels; and Examination Category N-3, Removable Core Support Structures

VII-1.4.8.1 Visual Examination, VT-1. The following relevant conditions² shall require corrective action to meet the requirements of VII-1.3.1.2(b) prior to service or VII-1.3.1.4(b) prior to continued service:

(a) crack-like surface flaws on the welds joining the attachment to the vessel wall that exceed the allowable linear flaw standards of VII-1.4.1, or

(b) structural degradation of attachment welds such that the original cross-sectional area⁴ is reduced by more than 10%

VII-1.4.8.2 Visual Examination, VT-3. The following relevant conditions² shall require corrective action in meeting the requirements of VII-1.3.1.2(b) prior to service or VII-1.3.1.4(b) prior to continued service:

(a) structural distortion or displacement of parts to the extent that component function may be impaired

(b) loose, missing, cracked, or fractured parts, bolting, or fasteners

(c) foreign materials or accumulation of corrosion products that could interfere with control rod motion or could result in blockage of coolant flow through fuel

(d) corrosion or erosion that reduces the nominal section thickness by more than 5%

(e) wear of mating surfaces that may lead to loss of function, or

(f) structural degradation of interior attachments such that the original cross-sectional area is reduced more than 5%

VII-1.4.9 Standards for Examination Category P, All Pressure-Retaining Components

VII-1.4.9.1 Visual Examination, VT-2. Relevant conditions do not include conditions that result in condensation on components, normal collection of fluid in sumps, and drips from open drains. A component whose visual examination (IWA-5240 Division 1) detects any of the following relevant conditions shall meet VII-1.3.1.4(b) and IWA-5250 prior to continued service:

(a) any through-wall or through-weld, pressure-retaining material leakage from insulated and noninsulated components

(b) nonbored water leakage in excess of limits established by the Owner from mechanical connections (such as pipe caps, bolted connections, or compression fittings)

(c) areas of general corrosion of a component resulting from leakage

(d) leakage in excess of limits established by the Owner from components provided with leakage limiting devices (such as valve packing glands or pump seals)

(e) boded water leakage or evidence of boded water leakage (discoloration or accumulated residues on surfaces of components, insulation, or floor areas) not addressed in (a) or (d); or

(f) leakage or flow test results from buried components in excess of limits established by the Owner

VII-1.4.10 Standards for Examination Category O for Pressure-Retaining Welds in Control Rod Drive and Instrument Nozzle Housings

VII-1.4.10.1 Allowable Planar Flaws

(a) The size of an allowable planar flaw within the boundary of the examination surfaces and volumes delineated in Division 1, Figure IWB-2500-18 shall not exceed the limits specified in VII-1.4.10.2 and VII-1.4.10.3, as applicable.

(b) Where a flaw extends beyond the boundaries of the examination surfaces and volumes, or separate flaws are detected that lie both within and beyond the boundaries but are characterized as a single flaw by the requirements of Division 1, IWA-3300, the overall flaw size shall be compared with the standards of (a).

(c) Any two or more coplanar aligned flaws characterized as separate flaws by IWA-3300 are allowable, provided the requirements of Division 1, IWA-3390 are met.

VII-1.4.10.2 Allowable Flaw Standards for Surface Examination

(a) The length of allowable flaws shall not exceed $\frac{3}{16}$ in. (5 mm) for the preservice examination and $\frac{1}{4}$ in. (6 mm) for the inservice examination.

(b) Where a flaw on the outer surface of the housing exceeds the allowable standards, the housing may be examined using the volumetric method, and the acceptance standards of VII-1.4.10.3 shall apply.

VII-1.4.10.3 Allowable Flaw Standards for Volumetric Examination

(a) The depth of an allowable preservice flaw shall not exceed 10% of weld thickness; the length shall not exceed 60% of weld thickness.

(b) The depth of an allowable inservice flaw shall not exceed 12.5% of weld thickness; the length shall not exceed 75% of weld thickness.

VII-1.4.11 Standards for Examination Category F-A for Supports

VII-1.4.11.1 Acceptance by Examination. Component supports whose examinations do not reveal conditions described in VII-1.4.11.4(a) shall be acceptable for continued service. Confirmed changes in conditions from prior examinations shall be recorded in accordance with RIM-1.4(h).

VII-1.4.11.2 Acceptance by Corrective Measures or Repair/Replacement Activity. A support whose examination detects conditions described in VII-1.4.11.4(a) is unacceptable for continued service until such conditions are corrected by one or more of the following:

- (a) adjustment and reexamination for conditions such as
 - (1) detached or loosened mechanical connections
 - (2) improper hot or cold settings of spring supports and constant load supports
 - (3) misalignment of supports; or
 - (4) improper displacement settings of guides and stops
- (b) repair/replacement activities in accordance with Article IWA-4000 and reexamination

VII-1.4.11.3 Acceptance by Evaluation or Test

(a) As an alternative to the requirements of VII-1.4.11.2, a component support or a portion of a component support containing relevant conditions that do not meet the acceptance standards of VII-1.4.11.4 shall be acceptable for service without corrective actions if an evaluation or test demonstrates that the component support is acceptable for service.

(b) If a component support or a portion of a component support has been evaluated or tested and determined to be acceptable for service in accordance with (a), the

Owner may perform corrective measures to restore the component support to its original design condition.

VII-1.4.11.4 Acceptance Standards — Component Support Structural Integrity

(a) Component support conditions that are unacceptable for continued service shall include the following:

- (1) deformations or structural degradations of fasteners, springs, clamps, or other support items
- (2) missing, detached, or loosened support items
- (3) arc strikes, weld spatter, paint, scoring, roughness, or general corrosion on close tolerance machined or sliding surfaces
- (4) improper hot or cold settings of spring supports and constant load supports
- (5) misalignment of supports
- (6) improper clearances of guides and stops
- (7) evidence of fluid leakage from viscoelastic dampers

(b) Except as defined in (a), the following are examples of nonrelevant conditions:

- (1) fabrication marks (e.g., from punching, layout, bending, rolling, and machining)
- (2) chipped or discolored paint
- (3) weld spatter on other than close tolerance machined or sliding surfaces
- (4) scratches and surface abrasion marks
- (5) roughness or general corrosion which does not reduce the load bearing capacity of the support
- (6) general conditions acceptable by the material, Design, and/or Construction Specifications

VII-1.5 ANALYTICAL EVALUATION OF PLANAR FLAWS (21)

(a) A flaw that exceeds the size of allowable flaws defined in VII-1.4 may be analytically evaluated using procedures described in this subarticle to calculate flaw growth until the next inspection or the end of the service lifetime of the component or piping item.

(b) For purposes of analytical evaluation, the depth of flaws in clad components and piping items shall be defined in accordance with Division 1, Figure IWB-3600-1 as follows:

- (1) Category 1 — A flaw that lies entirely in the cladding, as shown in Figure IWB-3600-1, need not be analytically evaluated.
- (2) Category 2 — A surface flaw that penetrates the cladding and extends into the ferritic steel shall be analytically evaluated on the basis of the total flaw depth in both the ferritic steel and the cladding as shown in Figure IWB-3600-1.
- (3) Category 3 — A subsurface flaw that lies in both the ferritic steel and the cladding shall be treated as either a surface or a subsurface flaw depending on the relationship between S and d as shown in Figure IWB-3600-1.

(4) Category 4 — A subsurface flaw that lies entirely in the ferritic steel and terminates at the weld metal interface shall be treated as either a surface or subsurface flaw depending on the relationship between S and d as shown in Figure IWB-3600-1.

(5) Category 5 — A subsurface flaw contained entirely in the ferritic steel shall be treated as either a surface or a subsurface flaw depending on the relationship between S and d as shown in Figure IWB-3600-1.

(c) The flaw characterization rules of Division 1, IWA-3300 shall be used for transformation of a subsurface flaw to a surface flaw using dimensions S and d illustrated in Figure IWB-3600-1.

(d) When examination results do not permit accurate determination of the flaw category, a more conservative category shall be selected.

(21) VII-1.5.1 Acceptance Criteria for Ferritic Steel Components 4 in. (100 mm) and Greater in Thickness

(a) A flaw that exceeds the size of allowable flaws defined in VII-1.4.1 and VII-1.4.2 may be analytically evaluated using procedures such as those described in Division 1, Nonmandatory Appendix A to calculate its growth until the next inspection or the end of service lifetime of the component.

(b) The component containing the flaw is acceptable for continued service during the evaluated time period if the following are satisfied:

(1) the criteria of VII-1.5.1.1 or VII-1.5.1.2

(2) the primary stress limits of the Construction Code, assuming local area reduction of the pressure-retaining membrane that is equal to the area of the detected flaws as determined by the flaw characterization requirements of Division 1, IWA-3000

(c) The analytical evaluation procedures shall be the responsibility of the Owner.

VII-1.5.1.1 Acceptance Criteria Based on Flaw Size. A flaw exceeding the limits of VII-1.4 is acceptable if the critical flaw parameters satisfy the following criteria:

$$a_f < 0.1a_c$$

$$a_f < 0.5a_i$$

where

a_c = minimum critical size of the flaw under normal operating conditions

a_f = maximum size to which the detected flaw is calculated to grow in a specified time period, which can be the next scheduled inspection of the component, or until the end of vessel design lifetime

a_i = minimum critical size of the flaw for initiation of non-arresting growth under postulated emergency and faulted conditions

VII-1.5.1.2 Acceptance Criteria Based on Applied Stress Intensity Factor. A flaw exceeding the limits of VII-1.4 is acceptable if the applied stress intensity factor for the flaw dimensions a_f and l_f satisfies the following criteria:

(a) For normal conditions

$$K_I < K_{Ic} / \sqrt{10}$$

where

K_I = applied stress intensity factor for normal conditions, including upset and test conditions for the flaw dimensions a_f and l_f

a_f = end-of-evaluation-period flaw depth defined in VII-1.5.1.1

l_f = end-of-evaluation-period flaw length

K_{Ic} = fracture toughness based on crack initiation for the corresponding crack-tip temperature

(b) For emergency and faulted conditions

$$K_I < K_{Ic} / \sqrt{2}$$

where

K_I = applied stress intensity factor under emergency and faulted conditions for flaw dimensions a_f and l_f

VII-1.5.1.3 Acceptance Criteria for Flanges and Shell Regions Near Structural Discontinuities. The following criteria shall be used for the analytical evaluation of flaws in areas of structural discontinuity, such as vessel flange and nozzle-to-shell regions. A flaw exceeding the limits of VII-1.4 is acceptable if the applied stress intensity factor for the dimensions a_f and l_f satisfies the following limits:

(a) For conditions where pressurization does not exceed 20% of the Design Pressure, during which the minimum temperature is not less than RT_{NDT}

$$K_I < K_{Ic} / \sqrt{2}$$

where

K_I = applied stress intensity factor for flaw dimensions a_f and l_f

a_f = end-of-evaluation-period flaw depth defined in VII-1.5.1.1

l_f = end-of-evaluation-period flaw length

K_{Ic} = fracture toughness based on crack initiation for the corresponding crack-tip temperature

(b) For normal conditions (including upset and test conditions), excluding those described in (a), the criteria of VII-1.5.1.1 or VII-1.5.1.2(a) shall be satisfied.

(c) For emergency and faulted conditions, the criteria of VII-1.5.1.1 or VII-1.5.1.2(b) shall be satisfied.

VII-1.5.2 Acceptance Criteria for Ferritic Components Less Than 4 in. (100 mm) in Thickness

These criteria are in the course of preparation. In the interim, the criteria of VII-1.5.1 may be applied.

(21) VII-1.5.3 Analytical Evaluation Procedures and Acceptance Criteria for Flaws in Austenitic and Ferritic Piping

Piping containing flaws exceeding the acceptance standards of VII-1.4.3 may be analytically evaluated to determine acceptability for continued service to the next inspection or to the end of the evaluation period. For purposes of analytical evaluation, the depth of flaws in clad piping items shall be defined in accordance with Division 1, Figure IWB-3600-1. The flaw characterization rules of Division 1, IWA-3300 shall be used for the transformation of a subsurface flaw to a surface flaw using dimensions S and d . A pipe containing flaws is acceptable for continued service for a specified evaluation time period if the criteria of VII-1.5.3.2, VII-1.5.3.3, or VII-1.5.3.4 are satisfied. The procedures shall be the responsibility of the Owner.

VII-1.5.3.1 Analytical Evaluation Procedures. Analytical evaluation procedures based on flaw size or applied stress, such as those described in Division 1, Nonmandatory Appendix C or Nonmandatory Appendix H, may be used, subject to the following:

(a) The analytical evaluation procedures and acceptance criteria in Division 1, Nonmandatory Appendix C are applicable to piping NPS 1 (DN25) and greater. The procedures and criteria in Division 1, Nonmandatory Appendix H are applicable to piping NPS 4 (DN 100) and greater. Division 1, Nonmandatory Appendices C and H are applicable to portions of adjoining pipe fittings within a distance of $(R_2t)^{1/2}$ from the weld centerline, where R_2 is the outside radius and t is the nominal thickness of the pipe. The weld geometry and weld-base metal interface are defined in Division 1, Nonmandatory Appendix C.

(b) The analytical evaluation procedures and acceptance criteria are applicable to seamless or welded wrought carbon steel pipe and pipe fittings, and associated weld materials that have a specified minimum yield strength not greater than 40 ksi (280 MPa).

(c) The analytical evaluation procedures and acceptance criteria are applicable to seamless or welded wrought or cast austenitic pipe and pipe fittings and associated weld materials that are made of wrought stainless steel, Ni-Cr-Fe alloy, or cast stainless steel, and have a specified minimum yield strength not greater than 45 ksi (310 MPa).

(d) A flaw growth analysis shall be performed on the detected flaw to predict its growth due to fatigue or stress corrosion cracking mechanisms, or both, when applicable,

during a specified evaluation time period. The time interval selected for flaw growth analysis (i.e., evaluation period) shall be until the next inspection or until the end of the evaluation period for the item.

(e) The calculated maximum flaw dimensions at the end of the evaluation period shall be compared to the acceptance criteria for Service Levels A, B, C, and D loadings to determine the acceptability of the item for continued service.

VII-1.5.3.2 Analytical Evaluation Procedures and Acceptance Criteria Based on Failure Mode Determination. Piping containing flaws exceeding the acceptance standards of VII-1.4.3.1 may be analytically evaluated using analytical procedures described in Division 1, Nonmandatory Appendix C and is acceptable for continued service during the evaluated time period when the critical flaw parameters satisfy the criteria in Division 1, Nonmandatory Appendix C. Flaw acceptance criteria are based on allowable flaw size or allowable stress. Flaws with depths greater than 75% of the wall thickness are unacceptable.

VII-1.5.3.3 Analytical Evaluation Procedures and Acceptance Criteria Based on Use of a Failure Assessment Diagram. Piping containing flaws exceeding the allowable flaw standards of VII-1.4.3.1 may be analytically evaluated using procedures based on use of a failure assessment diagram, such as described in Division 1, Nonmandatory Appendix H. Such analytical evaluation procedures may be invoked in accordance with the conditions of VII-1.5.3.1. Flaws with depths greater than 75% of the wall thickness are unacceptable.

VII-1.5.3.4 Alternative Analytical Evaluation Procedure and Acceptance Criteria Based on Applied Stress. Piping containing flaws exceeding the allowable flaw standards of VII-1.4.3.1 is acceptable for continued service until the end of the evaluation period if the alternative analytical evaluation procedure demonstrates, at the end-of-evaluation period, structural factors, based on load, equivalent to the following:

Service Level	Structural Factor
A	2.7
B	2.4
C	1.8
D	1.4

Flaws with depths greater than 75% of the wall thickness are unacceptable.

VII-1.5.4 Evaluation Procedure and Acceptance Criteria for PWR Reactor Vessel Head Penetration Nozzles

PWR reactor vessel upper and lower head penetration nozzles containing flaws may be evaluated to determine acceptability for continued service in accordance with the

evaluation procedure and acceptance criteria of this paragraph. The evaluation procedures and acceptance criteria shall be the responsibility of the Owner.

Note that the acceptance standards of VII-1.4 shall not be used to accept indications in this region.

VII-1.5.4.1 Evaluation Procedure. This evaluation procedure is applicable to head penetration nozzles with 8 in. (200 mm) nominal outside diameter and less. This procedure shall not be used for partial penetration nozzle to vessel (J-groove) welds.

VII-1.5.4.2 Methodology for Evaluation

(a) A flaw growth analysis shall be performed on each detected flaw to determine its maximum growth due to fatigue, stress corrosion cracking or both mechanisms, when applicable, during a specified evaluation period. The minimum time interval for the flaw growth evaluation shall be until the next inspection.

(b) All applicable loadings shall be considered, including weld residual stress, in calculating the crack growth.

(c) The flaw shall be characterized in accordance with the requirements of Division 1, IWA-3400, including the proximity requirements of Figure IWA-3400-1 for surface flaws.

(d) The flaw shall be projected into both axial and circumferential orientations, and each orientation shall be evaluated. The axial orientation is the same for each nozzle, but the circumferential orientation will vary depending on the angle of intersection of the penetration nozzle with the head. The circumferential orientation is defined in Division 1, Figure IWB-3662-1.

(e) The location of the flaw, relative to the J-groove attachment weld, shall be determined.

(f) The flaw shall be evaluated using procedures such as those described in Division 1, Nonmandatory Appendix O, to calculate the following critical flaw parameters:

a_f = the maximum depth to which the detected flaw is calculated to grow at the end of the evaluation period

l_f = the maximum length to which the detected flaw is calculated to grow at the end of the evaluation period

VII-1.5.4.3 Acceptance Criteria. The calculated maximum flaw dimensions at the end of the evaluation period shall be compared with the maximum allowable flaw dimensions in Division 1, Table IWB-3663-1.

VII-1.6 ANALYTICAL EVALUATION OF PLANT OPERATING EVENTS

VII-1.6.1 Scope

This subarticle provides requirements for analytical evaluation of events and conditions for pressure boundary components and associated structures in operating plants.

VII-1.6.2 Unanticipated Operating Events

(a) When an operating event causes an excursion outside the normal operating pressure and temperature limits defined in the plant Technical Specifications, an analytical evaluation shall be performed to determine the effects of the out-of-limit condition on the structural integrity of the pressure boundary.

(b) The analytical evaluation procedures shall be the responsibility of the Owner.

VII-1.6.3 Fracture Toughness Criteria for Protection Against Failure

(a) During reactor operation, load and temperature conditions shall be maintained to provide protection against failure due to the presence of postulated flaws in the ferritic portions of the reactor coolant pressure boundary. Division 1, Nonmandatory Appendix G provides analytical evaluation procedures that may be used to define these load and temperature conditions.

(b) For reactor vessels with material upper shelf Charpy impact energy levels less than 50 ft-lb (68 J), service and test conditions may be analytically evaluated, using current-geometry and material properties, to provide protection against ductile failure. Division 1, Nonmandatory Appendix K contains analytical evaluation procedures that may be used to demonstrate protection against ductile failure.

(c) The analytical evaluation procedures used to define protection against failure due to the presence of postulated flaws shall be the responsibility of the Owner.

VII-1.6.4 Operating Plant Fatigue Assessments

(a) Division 1, Nonmandatory Appendix L provides analytical evaluation procedures that may be used to assess the effects of thermal and mechanical fatigue concerns on component acceptability for continued service.

(b) Division 1, Nonmandatory Appendix L provides analytical evaluation procedures that may also be used when the calculated fatigue usage exceeds the fatigue usage limit defined in the original Construction Code.

ARTICLE VII-2

SUPPLEMENT FOR LIQUID METAL REACTOR-TYPE PLANTS

(In Course of Preparation)

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ARTICLE VII-3

SUPPLEMENT FOR HIGH-TEMPERATURE GAS REACTOR-TYPE PLANTS

VII-3.1 SCOPE

This Supplement shall be used to provide specific requirements to the RIM Program to identify and evaluate potentially active degradation mechanisms and other unique requirements to supplement the RIM Program.

(a) This Supplement shall only be used for High Temperature Gas Reactors.

(b) Division 1, Article IWA-3000 shall be used as reference information to support this Supplement and is referenced by this Supplement.

(c) This Supplement shall only be used when ferritic components are limited to a maximum Design Temperature of 700°F (370°C) and austenitic components are limited to a maximum Design Temperature of 800°F (426°C). However, for SA-533 type B class 1 (UNS K12539 1) and SA-508 grade 3, class 1 (UNS K12042 1) the following operating limits shall apply:

Temperature, °F (°C)	Time, hr	Number of Excursions
≤700 (≤370)	Design life	Unlimited
700–800 (370–425)	3,000 cumulative	Unlimited
800–1,000 (425–540)	1,000 cumulative	3 occurrences

VII-3.2 RIM PROGRAM — DAMAGE DEGRADATION ASSESSMENT

See Table VII-3.2-1.

VII-3.3 ACCEPTANCE STANDARDS

VII-3.3.1 Evaluation of Examination Results

VII-3.3.1.1 Preservice Volumetric and Surface Examinations

(a) General

(1) The preservice volumetric and surface examinations required by RIM-2.7.3 and performed in accordance with RIM-2.9 shall receive an NDE evaluation by comparing the examination results with the acceptance standards specified in (b).

(2) Acceptance of components for service shall be in accordance with (b) and (c).

(b) Acceptance

(1) A component whose volumetric or surface examination in accordance with RIM-2.7.3 meets (-a), (-b), or (-c) below, shall be acceptable for service, provided the verified flaws are recorded in accordance with the requirements of RIM-1.4(g) and RIM-2.9.2(a) in terms of location, size, shape, orientation, and distribution within the component.

(-a) The volumetric or surface examination (RIM-2.7.3) confirms the absence of flaws or identifies only flaws that have already been shown to meet the non-destructive examination standards of the Construction Code for materials or welds as applicable, documented in Quality Assurance Records.

(-b) Volumetric examination detects flaws that are confirmed by surface or volumetric examination to be non-surface-connected and that do not exceed the standards of Table VII-3.3.3-1.

(-c) Volumetric examination detects flaws that are confirmed by surface or volumetric examination to be non-surface-connected and that are accepted by analytical evaluation in accordance with the provisions of VII-3.3.1.3(b)(4) to the end of the service lifetime of the component and reexamined in accordance with the requirements of RIM-2.7.6.3(a) and RIM-2.7.6.3(b).

(2) A component whose volumetric or surface examination (RIM-2.7.3) detects flaws that do not meet the criteria established in (1) shall be unacceptable for service, unless the component is corrected by a repair/replacement activity in accordance with (c) to the extent necessary to meet the provisions of (1) prior to placement of the component in service.

(3) A component whose volumetric or surface examination (RIM-2.7.3) detects flaws, other than the flaws of (2), that exceed the standards of Table VII-3.3.3-1 is unacceptable for service, unless the component is corrected by a repair/replacement activity to the extent necessary to meet the acceptance standards prior to placement of the component in service.

(c) *Repair/Replacement Activity and Preservice Examination.* The repair/replacement activity and preservice examination shall comply with the requirements of Article RIM-4. Preservice examination shall be conducted in accordance with the requirements of RIM-2.9. The recorded results shall demonstrate that the area subjected

Table VII-3.2-1 Degradation Mechanism Attributes and Attribute Criteria

Degradation Mechanism	Attribute Criteria	Degradation Features and Susceptible Regions	Table VII-3.3.3-1 Examination Category
TF	TASCS - single pipe and operating temperature $>104^{\circ}\text{C}$ (220°F), and - piping $>\text{DN } 25$ (NPS 1), and - pipe segment has a slope $<45^{\circ}$ from horizontal (includes elbow or tee into a vertical pipe), and - potential exists for low flow in a pipe section connected to a component allowing mixing of hot and cold fluids, or - potential exists for leakage flow past a valve (i.e., in-leakage, out-leakage, cross-leakage) allowing mixing of hot and cold fluids, or - potential exists for convection heating in dead-ended pipe sections connected to a source of hot fluid, or - Potential exists for two phase (steam/water) flow, or - potential exists for turbulent penetration in branch pipe connected to header piping containing hot fluid with high turbulent flow, and - calculated or measured $\Delta T > 28^{\circ}\text{C}$ (50°F), and - Richardson Number >4.0 OR - Helium counterflow in dual pipe, and - Relatively high-velocity flow in the hotter pipe and relatively low velocity flow in the colder pipe, and - The difference between the fluid temperature in the hotter and colder pipes $>900^{\circ}\text{C}$ ($1,620^{\circ}\text{F}$)	cracks can initiate in welds, heat affected zones (HAZ), and base metal at the pipe inner surface affected locations can include nozzles, branch pipe connections, safe ends, and regions of stress concentration TASCS can occur over extensive portions of the pipe inner surface crack growth is relatively slow, and through-wall cracking is not expected within an inspection period	F, J, K
	TT - operating temperature $>132^{\circ}\text{C}$ (270°F) for stainless steel, or - operating temperature $>104^{\circ}\text{C}$ (220°F) for carbon steel, AND - potential for relatively rapid temperature changes including: - cold fluid injection into hot pipe segment, or - hot fluid injection into cold pipe segment, AND $\Delta T > 111^{\circ}\text{C}$ (200°F) for stainless steel, or $\Delta T > 83^{\circ}\text{C}$ (150°F) for carbon steel, or $\Delta T > \Delta T$ allowable or - allowable cycles $<10^6$		
VF	FIV - presence of attachments in a high velocity flow field, including: - welded attachments, or - attachments with small radii at the attachment junction - OR - high velocity cross flow over S/G or H/X tube bundles, and - absence of vibration damping tube supports	cracks can initiate in welds, HAZ, and base metal at the component inner or outer surface affected locations can include welded attachments and regions of stress concentration crack growth can be relatively fast, and through-wall cracks can occur within an inspection period	A, B, D, F, J, K, O as applicable NOTES: As approved by MANDEEP: - volumetric for part-through-wall cracks at the inner surface - surface for part-through-wall cracks at the outer surface and - leakage monitoring, leak testing, or visual for through-wall cracks
	MF - cyclic applied loads, and - presence of partial penetration welds, or - presence of small radii at the attachment junction - OR - presence of attached vibration sources (e.g., pumps, compressors) and - no preoperational vibration testing or monitoring, or - no vibratory monitoring of vibration sources during operation		
	SF - relative sliding motion between two contacting surfaces, and - absence of a solid lubricating system at the contacting surfaces	cracking, pitting, spalling wear, or seizing can occur at the contact surfaces cracking is expected to be localized and not grow through-wall	

Table VII-3.2-1 Degradation Mechanism Attributes and Attribute Criteria (Cont'd)

Degradation Mechanism		Attribute Criteria	Degradation Features and Susceptible Regions	Table VII-3.3.3-1 Examination Category
SCC	IGSCC	- BWR evaluated in accordance with existing plant IGSCC program per NRC Generic Letter 88-01 - OR - material is austenitic stainless-steel weld or HAZ, and - operating temperature $\geq 93^{\circ}\text{C}$ (200°F), and - susceptible material (carbon content $\geq 0.035\%$), and - oxygen or oxidizing species are present - OR - material is Alloy 82 or 182, and - operating temperature $\geq 93^{\circ}\text{C}$ (200°F), and - oxygen or oxidizing species are present - OR - material is austenitic stainless-steel weld or HAZ, and - operating temperature $< 93^{\circ}\text{C}$ (200°F), and - susceptible material (carbon content $\geq 0.035\%$), and - oxygen or oxidizing species are present, and - initiating contaminants (e.g., thiosulfate, fluoride, chloride) are present - OR - material is in an aqueous environment, and - oxygen or oxidizing species are present, and - mechanically induced high residual stresses are present	cracks can initiate in welds, and HAZ at the pipe inner surface affected locations can include pipe welds, branch pipe connections, and safe end attachment welds, crack growth is relatively slow, and through-wall cracking is not expected within an inspection period	A, B, D, F,G-1, G-2, J, K, O
	TGSCC	- material is austenitic stainless steel, and - operating temperature $> 65^{\circ}\text{C}$ (150°F), and - halides (e.g., fluoride, chloride) are present, or - caustic (NaOH) is present, and - oxygen or oxidizing species are present (only required to be present in conjunction w/halides, not required w/caustic)	cracks can initiate in welds, HAZ, and base metal at the pipe inner surface crack growth is relatively slow, and through-wall cracking is not expected within an inspection period	A, B, D, F,G-1, G-2, J, K, O
	ECSCC	- material is austenitic stainless steel, and - operating temperature $> 20^{\circ}\text{C}$ (68°F), and - an outside piping surface is within five diameters of a probable leak path (e.g., valve stems) and is covered with nonmetallic insulation that is not in compliance with USNRC Reg. Guide 1.36, or - piping surface is exposed to wetting from chloride bearing environments (e.g., seawater, sea spray, brackish water, brine) during fabrication, storage, or operation	cracks can initiate in welds, HAZ, and base metal at the pipe outer surface ECSCC can occur over extensive portions of the pipe inner or outer surface when exposed to wetting from chloride bearing environments during fabrication, storage or operation crack growth is relatively slow, and through-wall cracking is not expected within an inspection period	J, K
	PWSCC	- piping material is nickel-based alloy (e.g., alloy 600), and - exposed to primary water at $T > 298^{\circ}\text{C}$ (570°F), and - the material is mill-annealed and cold worked, or cold worked and welded without stress relief	cracks can initiate in welds, HAZ, and base metal at the pipe inner surface affected locations can include welds and HAZ without stress relief, the inside surface of nozzles, and areas of stress concentration crack growth can be relatively fast, and through-wall cracks can occur within an inspection period	F, J, K NOTES: leakage monitoring, leak testing, or visual for through-wall cracks as approved by MANDEEP

Table VII-3.2-1 Degradation Mechanism Attributes and Attribute Criteria (Cont'd)

Degradation Mechanism		Attribute Criteria	Degradation Features and Susceptible Regions	Table VII-3.3.3-1 Examination Category
HTC	C	– high temperature helium environment, and – graphite is present, and – no monitoring or control of impurities in the helium, and – component is carbon steel or low alloy steel with an operating temperature >350°C (662°F), or – component is austenitic stainless steel with an operating temperature >500°C (932°F)	cracks can initiate in welds, HAZ, and base metal at the component inner surface affected locations can include regions of the component exposed to the hot helium coolant flow stream degradation can occur over extensive portions of the pipe inner surface crack growth is relatively slow, and through-wall cracking is not expected within an inspection period	Volumetric methods as approved by MANDEEP
	CP	– operating temperature is higher than the allowable design temperature in ASME Section III	cracks can initiate in welds, HAZ, and base metal at the component inner surface affected locations can include areas of stress concentration crack growth is relatively slow, and through-wall cracking is not expected within an inspection period	
LC	MIC	– operating temperature <65°C (150°F), and – low or intermittent flow, and – pH <10, and – presence/intrusion of organic material (e.g., raw water system), or water source is not treated w/biocides and the water source is not demineralized water	cracking and wastage can initiate in welds, HAZ, base metal, and dissimilar metal joints (e.g., welds, flanges) at the component inner or outer surface MIC can occur over extensive portions of the pipe inner and outer surfaces crack growth is relatively slow, although through-wall cracks are expected	B, D, J, K NOTES: As approved by MANDEEP – volumetric for part-through-wall degradation at the inner surface and – visual for degradation at the outer surface
	PIT	– potential exists for low fluid flow, and – oxygen or oxidizing species are present, and – initiating contaminants (e.g., fluoride, chloride) are present	pitting can initiate in welds, HAZ, base metal at the component inner surface crack growth is relatively slow, but there is potential for through-wall pitting	Volumetric methods as approved by MANDEEP
	CC	– crevice condition exists, and – partial penetration weld attachments, or – regions with mechanically induced high residual stress, and – operating temperature >65°C (150°F), and – oxygen or oxidizing species are present	crevice corrosion can initiate in welds and HAZ at the component inner surface affected locations can include creviced regions with partial penetration welds or stress concentration crack growth is relatively slow, and through-wall cracking is not expected within an inspection period	Volumetric methods as approved by MANDEEP

Table VII-3.2-1 Degradation Mechanism Attributes and Attribute Criteria (Cont'd)

Degradation Mechanism		Attribute Criteria	Degradation Features and Susceptible Regions	Table VII-3.3.3-1 Examination Category
FS	E-C	- existence of cavitation sources (i.e., throttling or pressure reducing valves or orifices), and - helium environment, and - no monitoring or control of impurities in the helium flow stream, OR - existence of cavitation sources (i.e., throttling or pressure reducing valves or orifices), and steam environment, and - operating temperature <120°C (250°F), and - flow present >100 hr/yr, and - flow velocity >9.1 m/s (30 ft/s), and - $(P_d - P_v) / \Delta P < 5$	wall thinning can initiate in welds, HAZ, and base metal at the component inner surface affected locations can include regions up to one or two pipe diameters downstream of the cavitation source degradation growth is relatively slow, and through-wall degradation is not expected within an inspection period	B, J
	FAC	- carbon or low alloy steel piping with Cr < 1%, and - wet steam environment (i.e., coolant is not always dry or superheated steam), or - treated water environment, and - low levels of dissolved oxygen, and - high flow rate, and - turns in the flow path, and - pH < 9.5, and - fluid flow present >100 hr/yr	wall thinning can initiate in welds, HAZ, and base metal at the component inner surface affected locations can include regions where the potential for FAC degradation has been identified FAC can occur over extensive portions of the component inner surface degradation growth is relatively slow, and through-wall degradation is not expected within an inspection period	A, B, D, F, J, O
	PE	- solid particles in the helium flow stream, and - no monitoring or control of impurities and particle size (filtering) in the helium flow stream	wall thinning can initiate in welds, HAZ, and base metal at the component inner surface affected locations can include regions where the potential for PE degradation has been identified PE can occur over extensive portions of the component inner surface degradation growth is relatively slow, and through-wall degradation is not expected within an inspection period	B, D, F, J

Legend:

- C = carburization
 CP = creep
 CC = crevice corrosion
 DEP = degradation enhancement phenomena
 E-C = erosion-cavitation
 ECSCC = external chloride stress corrosion cracking
 FAC = flow-accelerated corrosion
 FIV = flow-induced vibration
 FS = flow sensitive
 HTC = high-temperature cracking
 IGSCC = intergranular stress corrosion cracking
 LC = localized corrosion
 LE = lowered emissivity
 LP = loose parts
 MF = mechanical fatigue
 MIC = microbiologically induced corrosion
 PE = particle erosion-corrosion
 PIT = pitting corrosion
 RE = radiation embrittlement
 RIA = restricted inspection access [Note (1)]